

Modelling of indirect steam gasification in circulating fluidized bed reactors

Kari Myöhänen¹, Juha Palonen², Timo Hyppänen¹

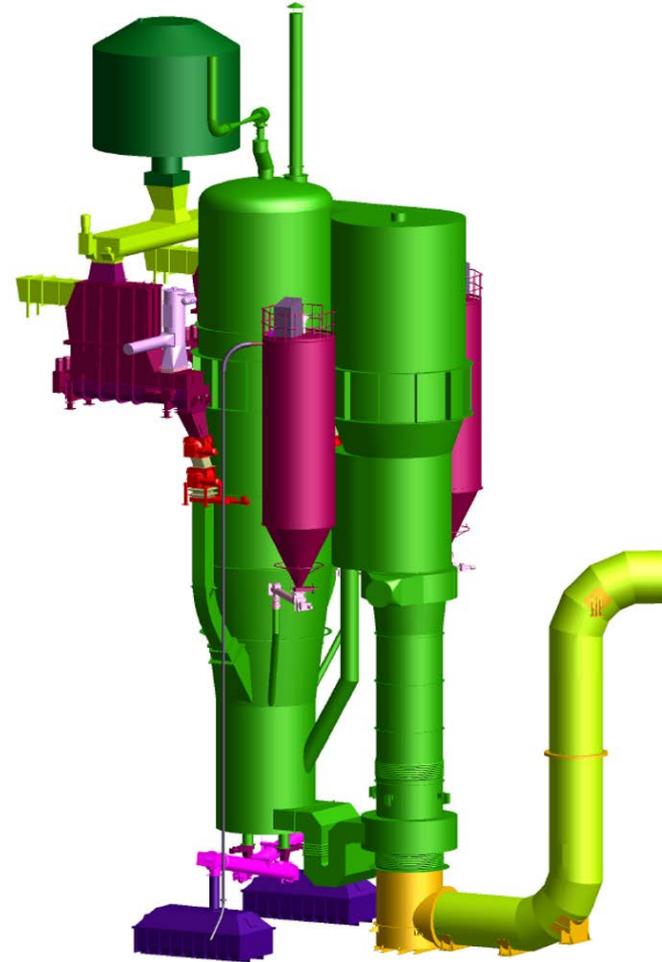
¹ LUT School of Energy Systems
Lappeenranta University of Technology

² AMEC Foster Wheeler Energia Oy, Finland



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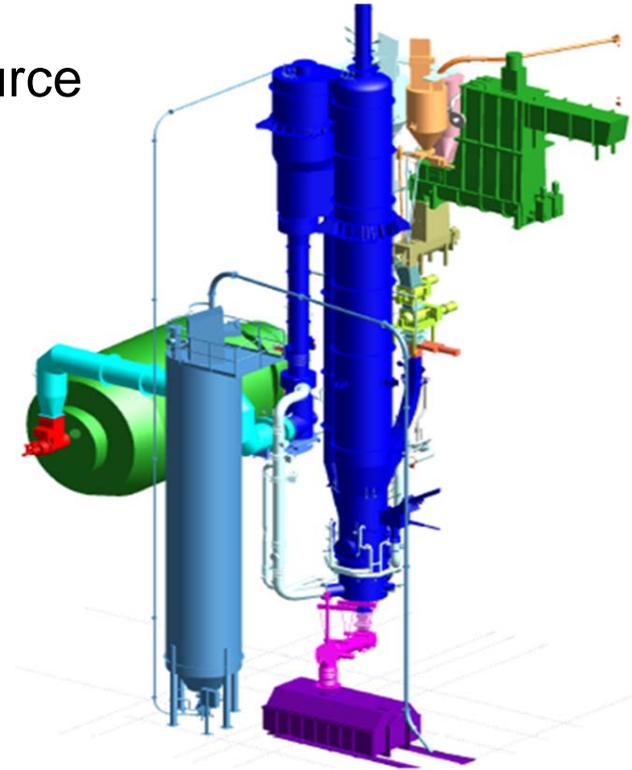
- Indirect steam gasification
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Design of a 140 MWth air-blown gasifier by AMEC Foster Wheeler

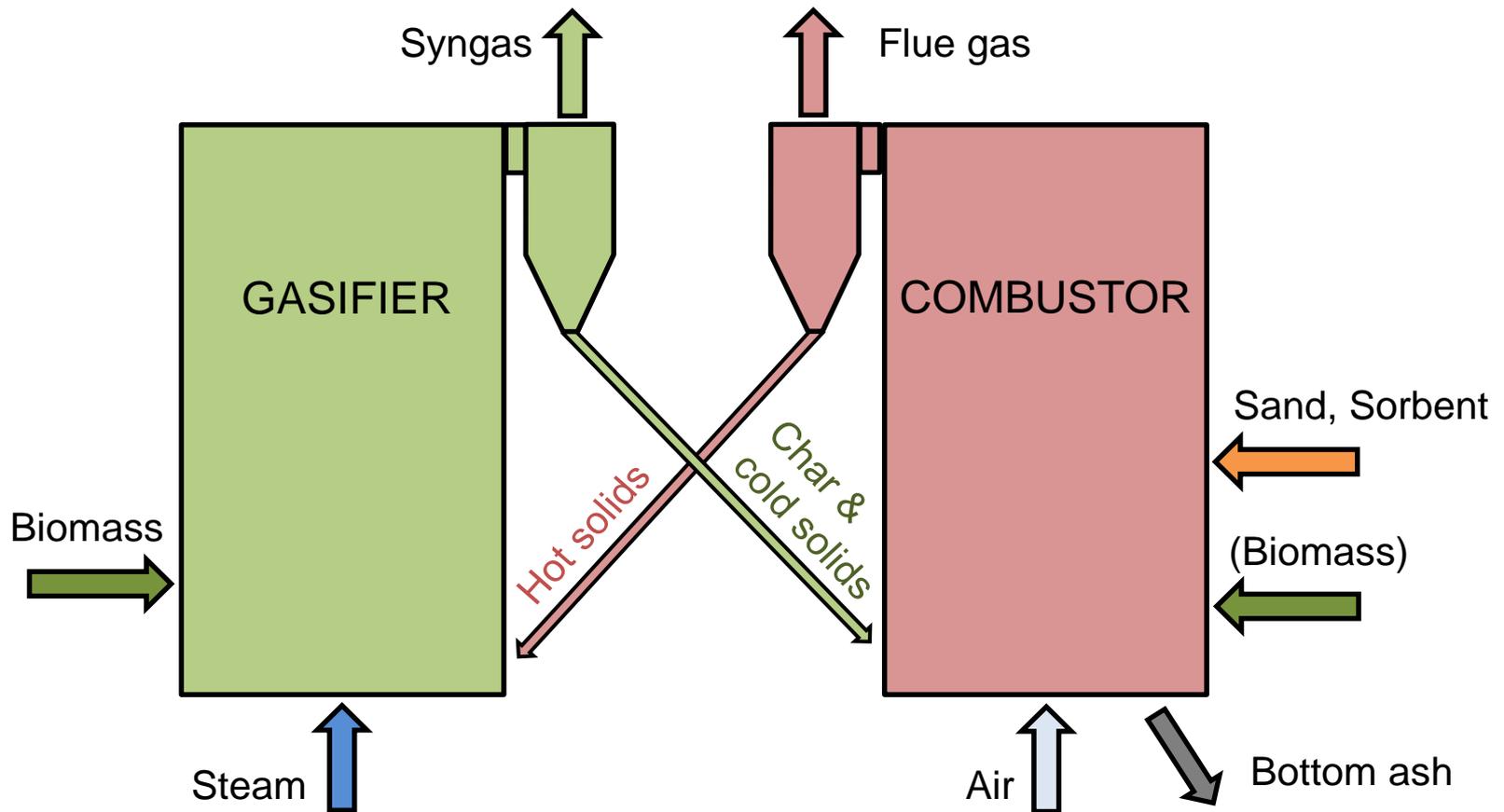
Biomass gasification

- Renewable, weather independent energy source
 - Gasification
 - Syngas (CO , H_2 , CO_2 , C_xH_y , H_2O)
 - SNG, FT-diesel, dimethyl ether, methanol, ...
- Modelling needed to support development of new process concepts and scale-up.
- Target of study:
development of modelling tool
for comprehensive simulation
of interconnected CFB processes
for indirect gasification.



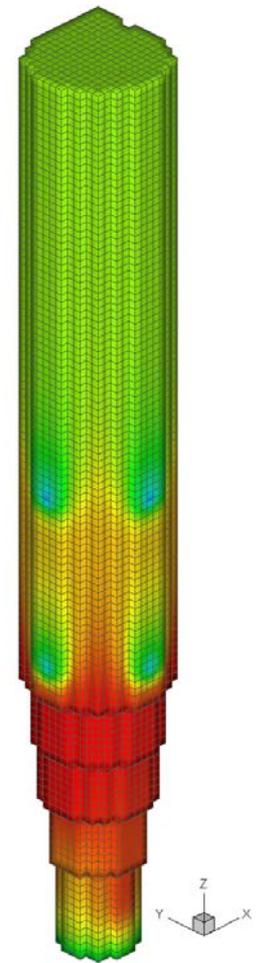
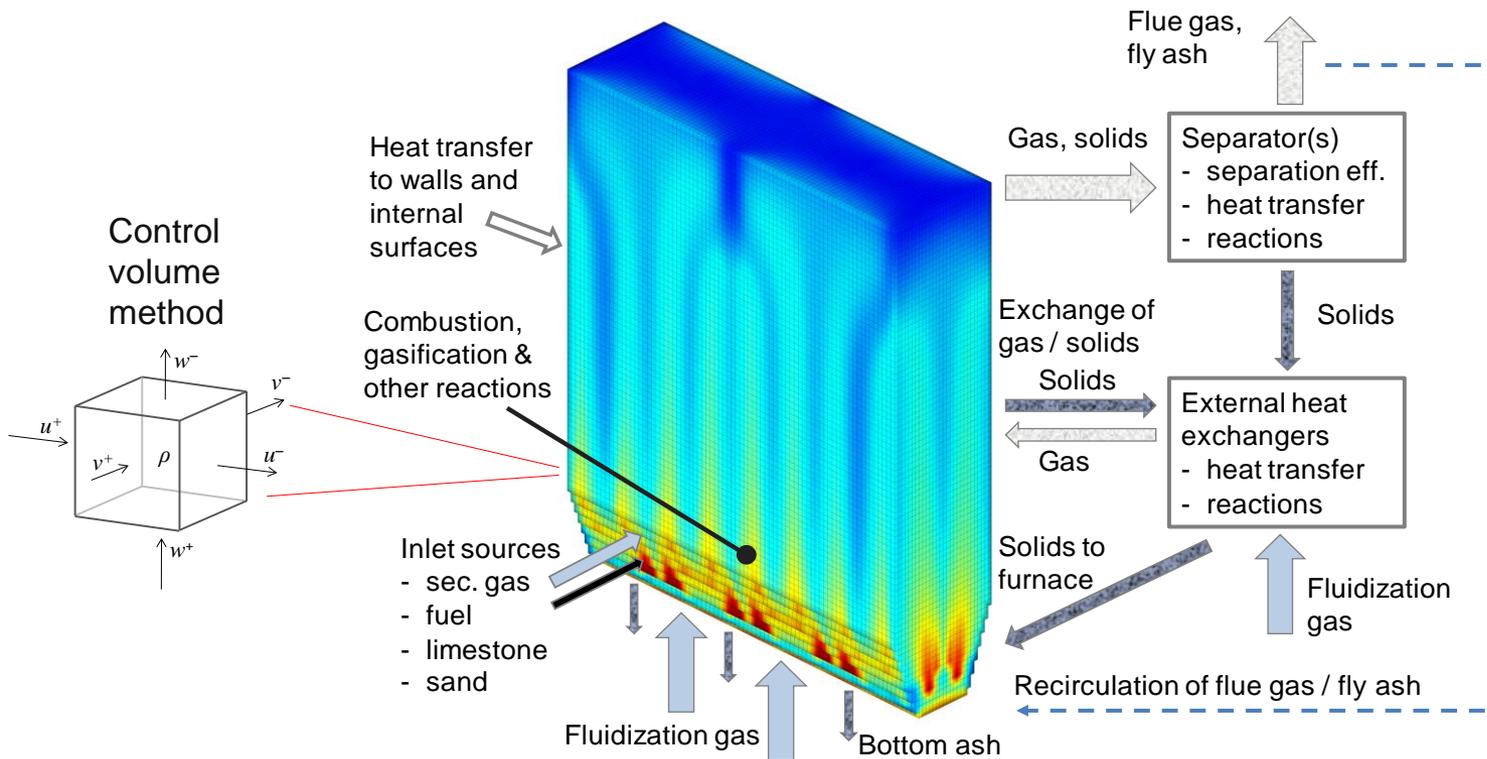
12 MWth lime kiln gasifier,
Stora Enso mill, Varkaus, Finland.

Indirect steam gasification



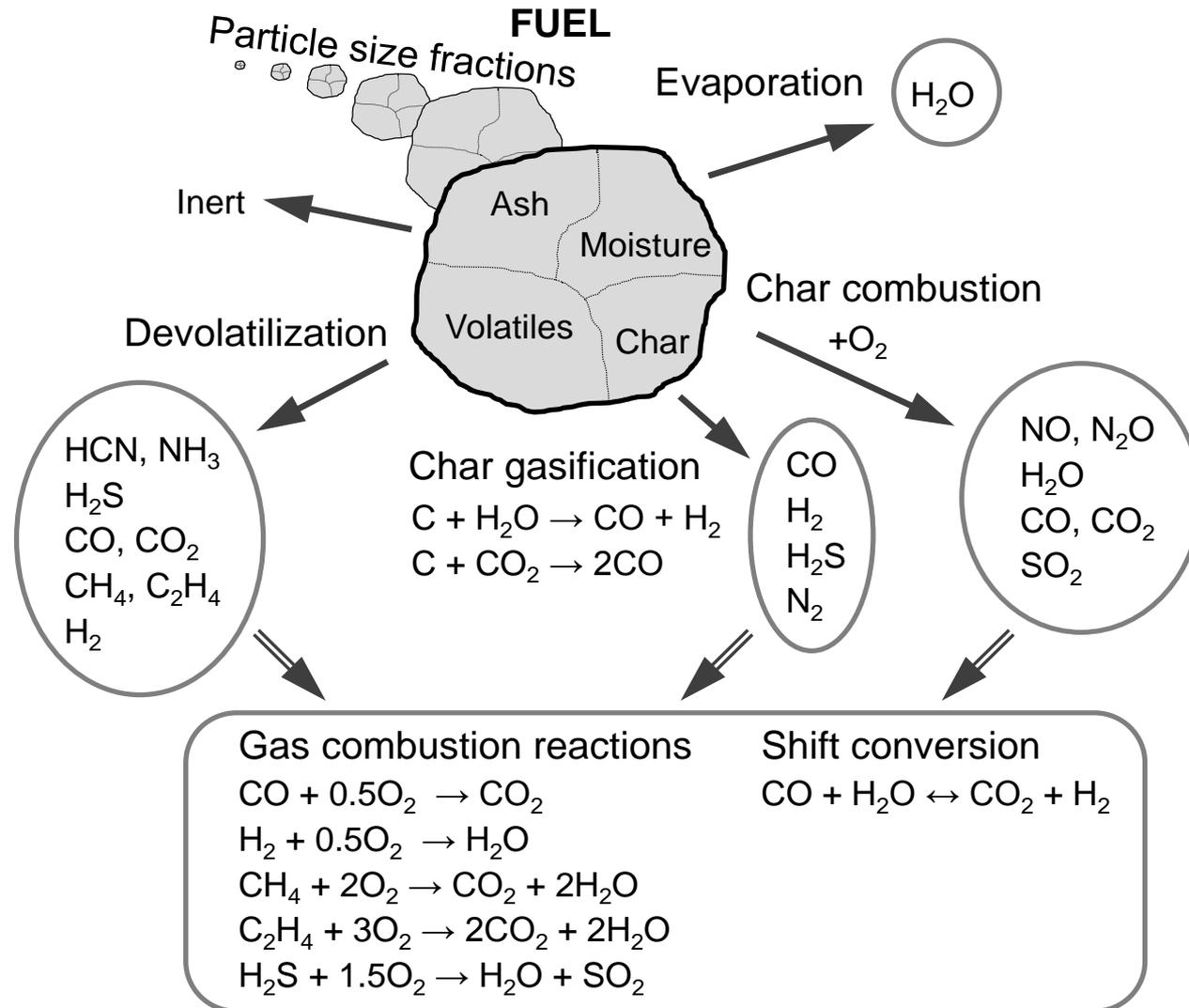
Three-dimensional model (CFB3D)

- In-house Fortran-code developed at LUT.
- Steady-state, semi-empirical engineering model.
- Applied for air/oxygen fired combustion, gasification, and calcium looping in bubbling and circulating fluidized bed processes.



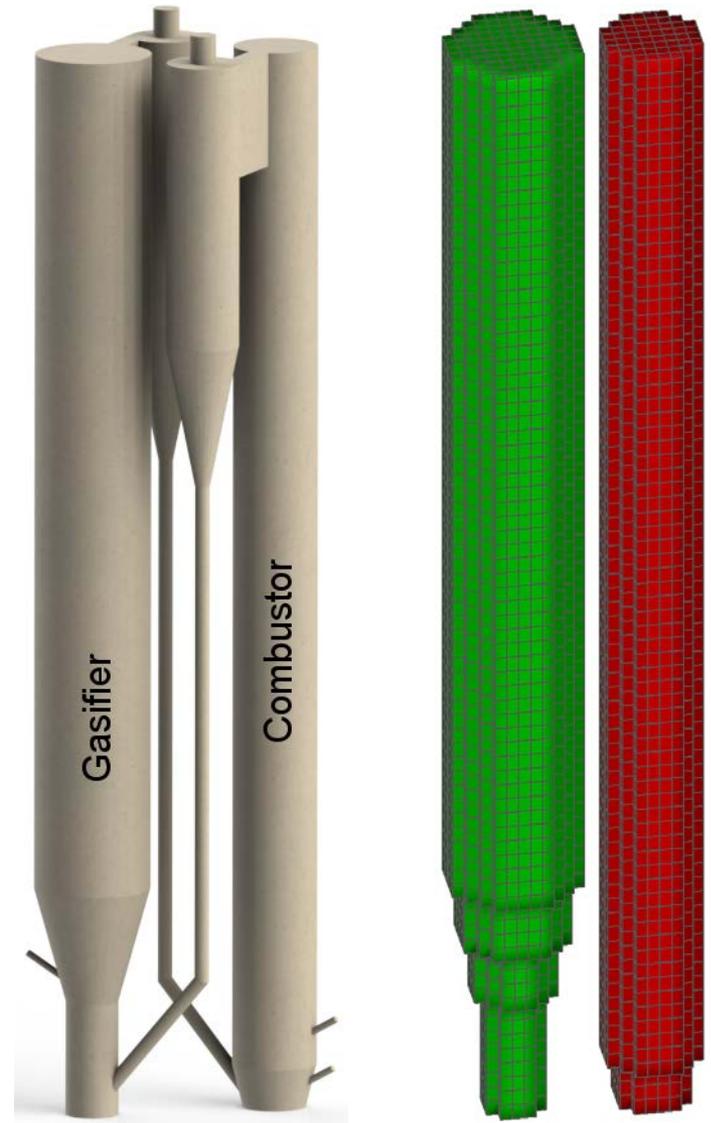
320 MWth gasifier
(6 bar, abs)

Modelled reaction system



Geometry and mesh

- Gasifier
 - Fuel input ≈ 12 MWth.
 - Diameter 1.6 m, height 15 m.
 - Fluidized by steam.
 - Woody biomass & secondary steam to level height 1.9 m.
- Combustor
 - Max. fuel input ≈ 2.1 MWth.
 - Diameter 1.4 m, height 15 m.
 - Fluidized by air.
 - Make-up sand, limestone, and secondary air to level 1.1 m.
 - Additional fuel feed to level 0.5 m.
- Reactors coupled in code.

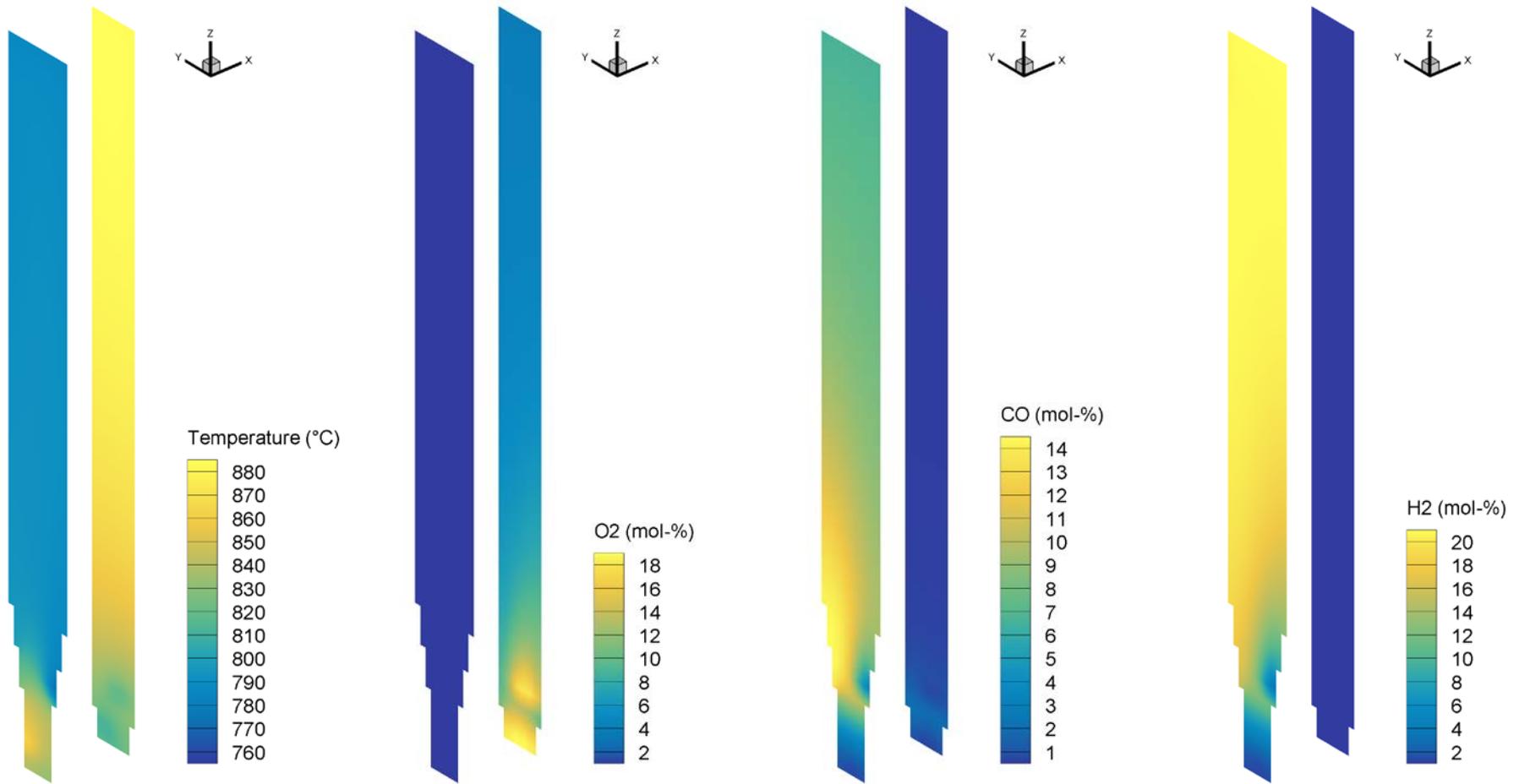


Boundary conditions

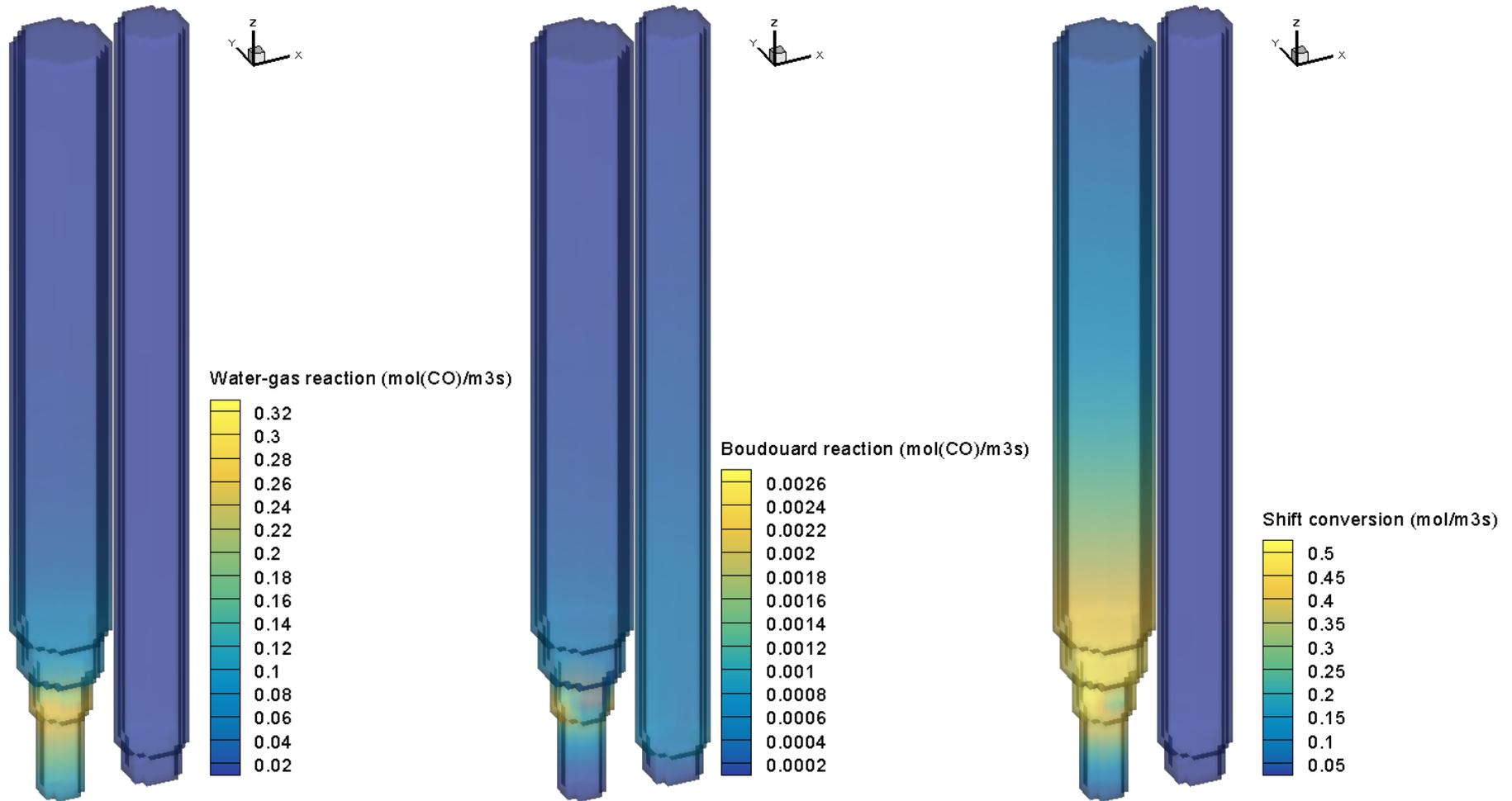
- Fuel = wood based biomass
 - 11% char, 62% volatiles, 25% moisture, LHV 14 MJ/kg,af.
- Four cases with varying fuel feed to combustor (0...2.1 MWth).
- Same excess oxygen in combustor in each case (3.94 %-vol,dry).

Parameter	Units	Case A01	Case A02	Case A03	Case A04
Steam flow to gasifier	(kg/s)	0.45
Primary steam ratio	(%)	40
Steam temperature	(°C)	180
Air flow to combustor	(kg/s)	1.84	2.06	1.62	1.38
Primary air ratio	(%)	50
Air temperature	(°C)	280
Fuel feed to gasifier	(kg/s)	0.9
Fuel feed to combustor	(kg/s)	0.10	0.15	0.05	0.00
Sand feed	(kg/s)	0.05
Limestone feed	(kg/s)	0.01
Solid feed temperatures	(°C)	30

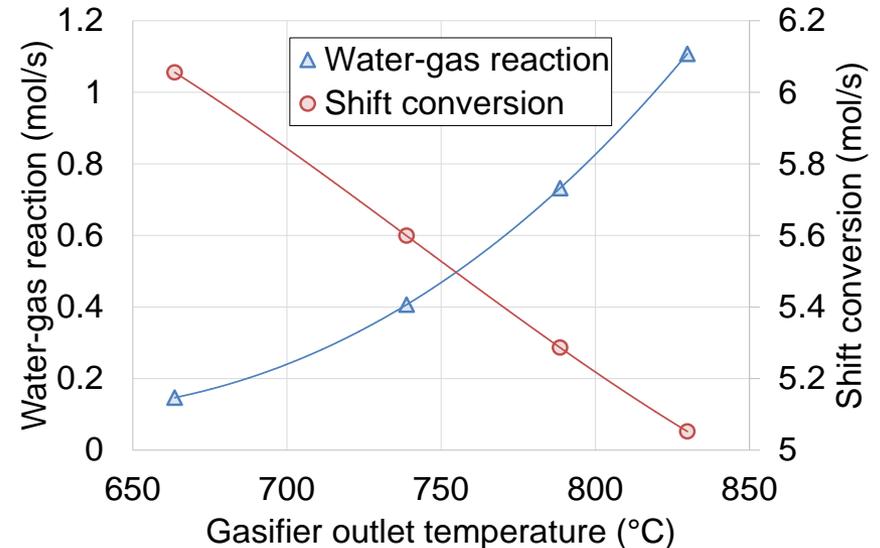
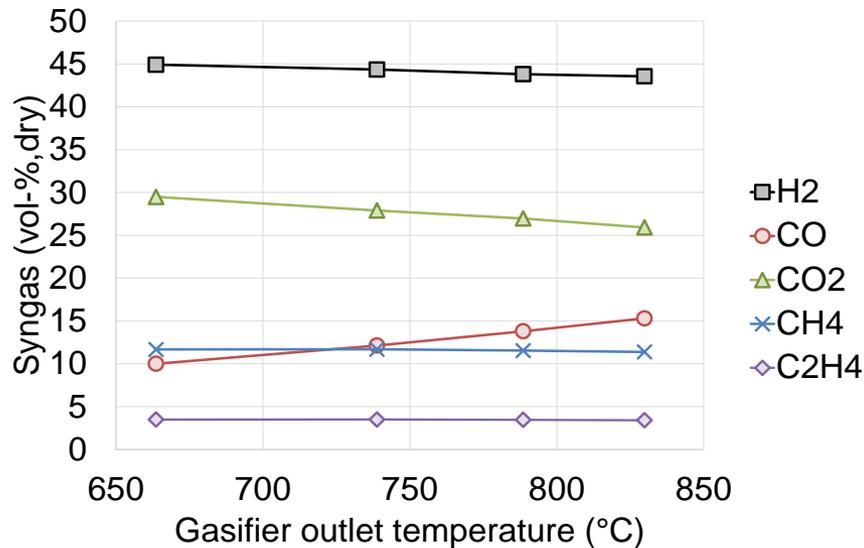
3D-model results at centre-plane, Case A01



Water-gas & Boudouard reaction and shift conversion (Case A01)



Syngas composition as function of temperature



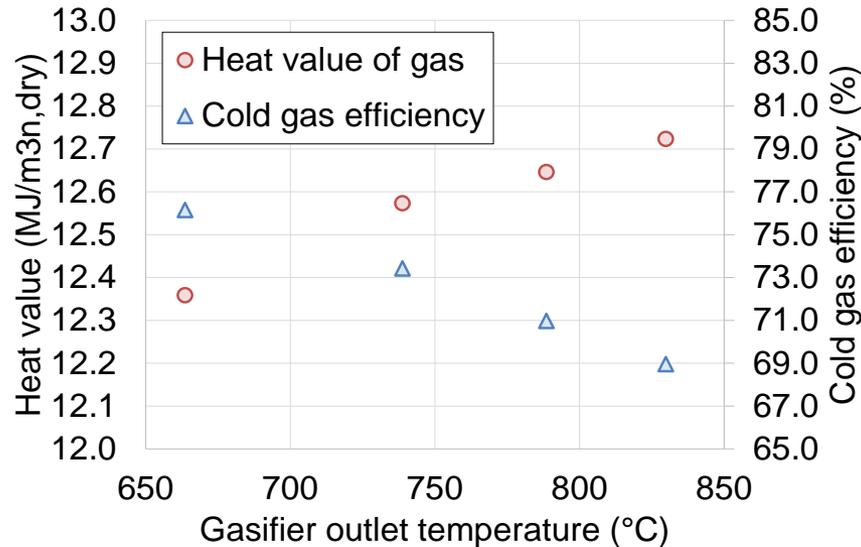
Increasing water-gas reaction ($C + H_2O \rightarrow CO + H_2$) → Higher CO & H₂

Decreasing shift conversion ($CO + H_2O \rightarrow CO_2 + H_2$) → Higher CO, lower CO₂ & H₂

Net effects as function of temperature:

- H₂ ≈ constant
- CO increasing
- CO₂ decreasing

Heat value of syngas and cold gas efficiency



$$\eta_{CG} = \frac{q_{v,gas} Q_{gas,LHV}}{\sum q_{m,fuel} Q_{fuel,LHV}}$$

Higher temperature → Higher gas yield from char

→ Increasing heat value of gas

(Opposite effect when compared with air- or oxy-fired gasification)

The increase in heat value of gas is smaller than the increase of fuel input

→ Decreasing cold gas efficiency

Summary

- Indirect steam gasification system with interconnected CFB reactors was successfully simulated by a semi-empirical model approach.
- Process can be operated without additional fuel feed to combustor.
- Effects of increasing the fuel feed to combustor:
 - Higher gasification temperature.
 - Slightly higher heat value of syngas.
 - Lower cold gas efficiency.
- Future targets:
 - Validation of model parameters based on measurement data.
 - Modelling of sorbent enhanced gasification (FLEDGED-project).

Thank you for your attention!

kari.myohanen@lut.fi

www.fledged.eu



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