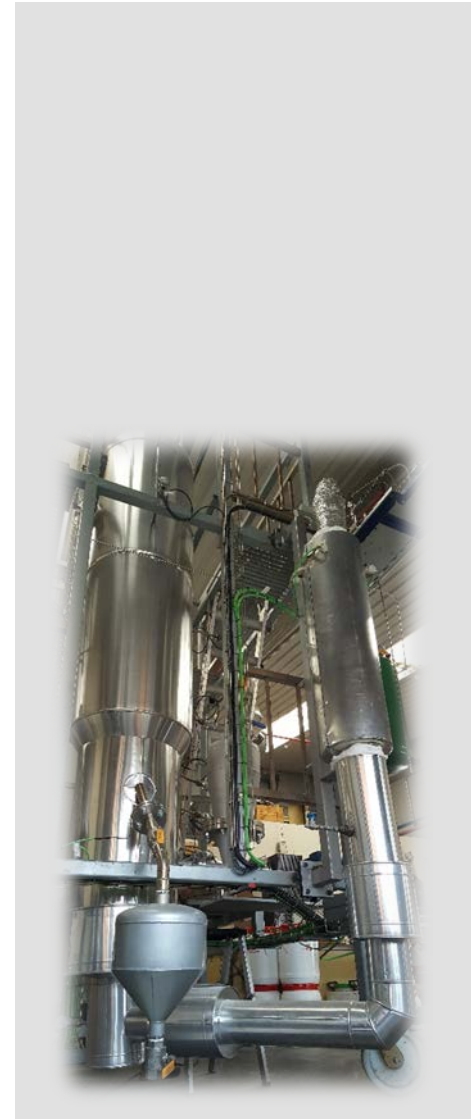


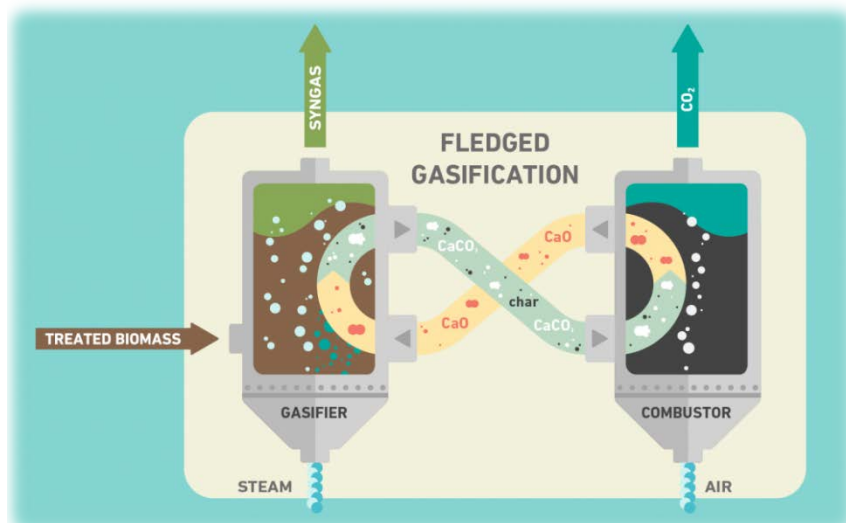
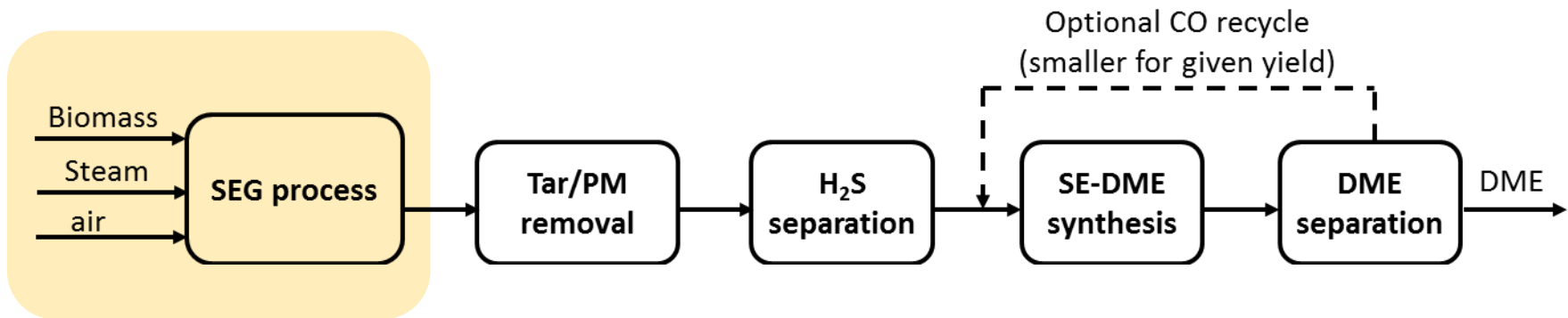
# Experimental investigation on sorption enhanced gasification (SEG) of biomass in a fluidized bed reactor for producing a tailored syngas

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- OBJECTIVE FLEDGED project: **Develop a highly intensified and flexible process for DME production from biomass and validate it under industrially relevant environments** (i.e. Technology Readiness Level 5 (TRL))



- Indirect gasification in a dual fluidized bed system using CaO as bed material
- Energy needed for gasification supplied by CaO carbonation ( $\rightarrow$  CaCO<sub>3</sub>) and by circulating solids
- Unconverted char leaving the gasifier supplies the energy needed in the combustor
- The presence of CaO simplifies the syngas cleaning and purification section

More info: <http://www.fledged.eu/>

## FUNDAMENTAL RESEARCH ON GASIFICATION OF DIFFERENT BIOMASSES AND DIFFERENT NATURAL SORBENTS

### ✓ Assessment of the enhanced gasification process in a bubbling fluidized bed reactor



- Test the different biomasses under different conditions of temperature, sorbent/fuel ratio and steam/carbon ratio.
- Influence of **type of sorbent** and the **activity** of the limestone (number of cycles)

Sorption enhanced gasification tests using grape seeds as biomass have been performed, analyzing the effect of the S/C ratio, the sorbent-to-biomass ratio and the activity of the sorbent on the syngas composition

### ○ Biomass: Grape seeds



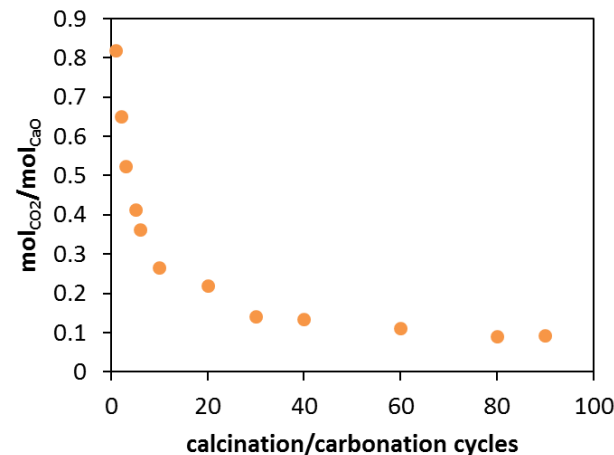
4.5-6.8 mm

Ultimate analysis [%wt.]		Proximate analysis [%wt.]	
C	53.92	Moisture	6.30
H	6.58	Volatile matter	65.12
N	2.20	Ash	4.30
S	0.12	Fixed carbon	24.28
O	32.35		
Cl	0.06	LHV [MJ/kg]	20.51

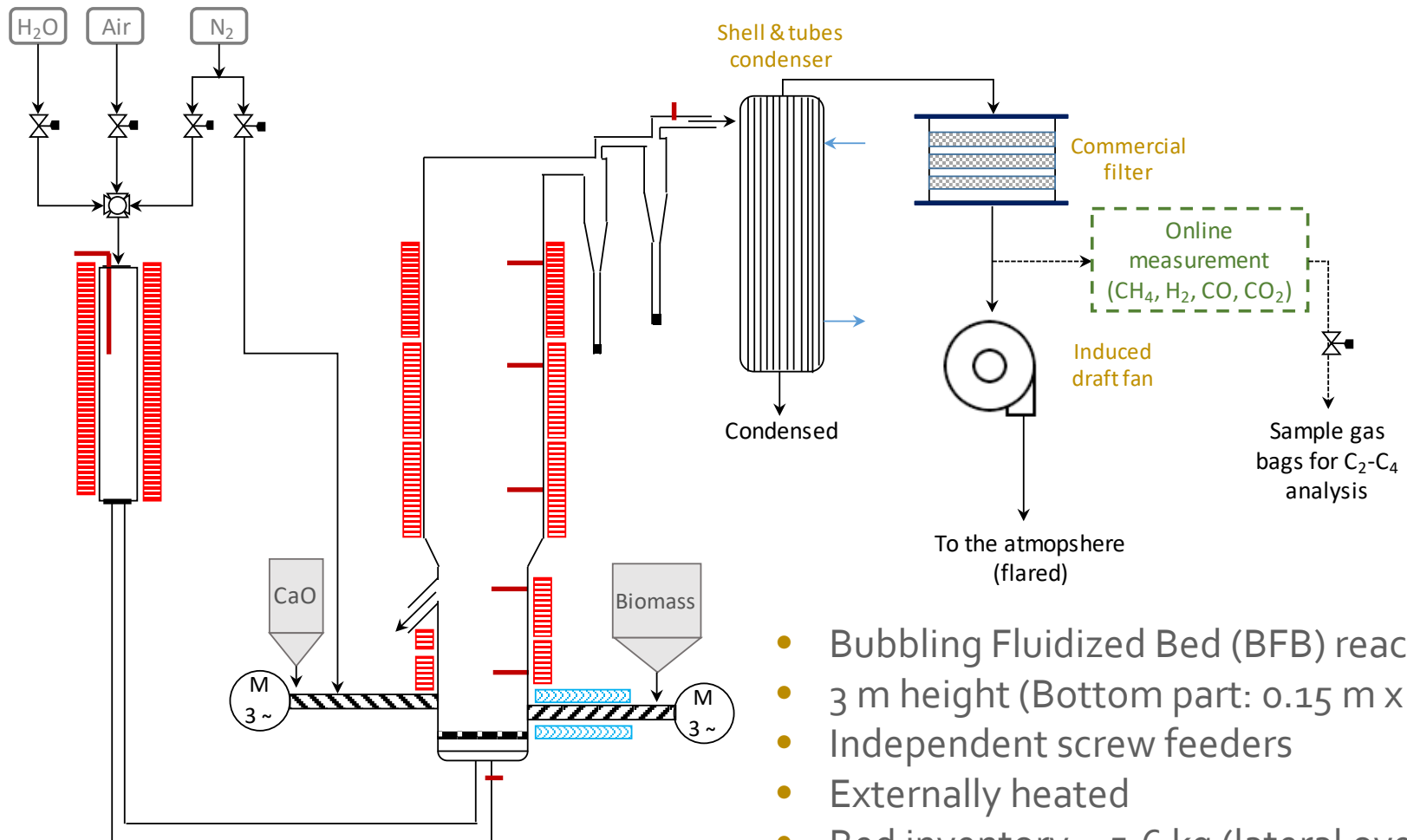
- Homogenous biomass
- High LHV (compared with PW or A1 pellets)
- Relatively low Ash and S contents (residual biomass)

### ○ CO<sub>2</sub> sorbent: Calcined limestone

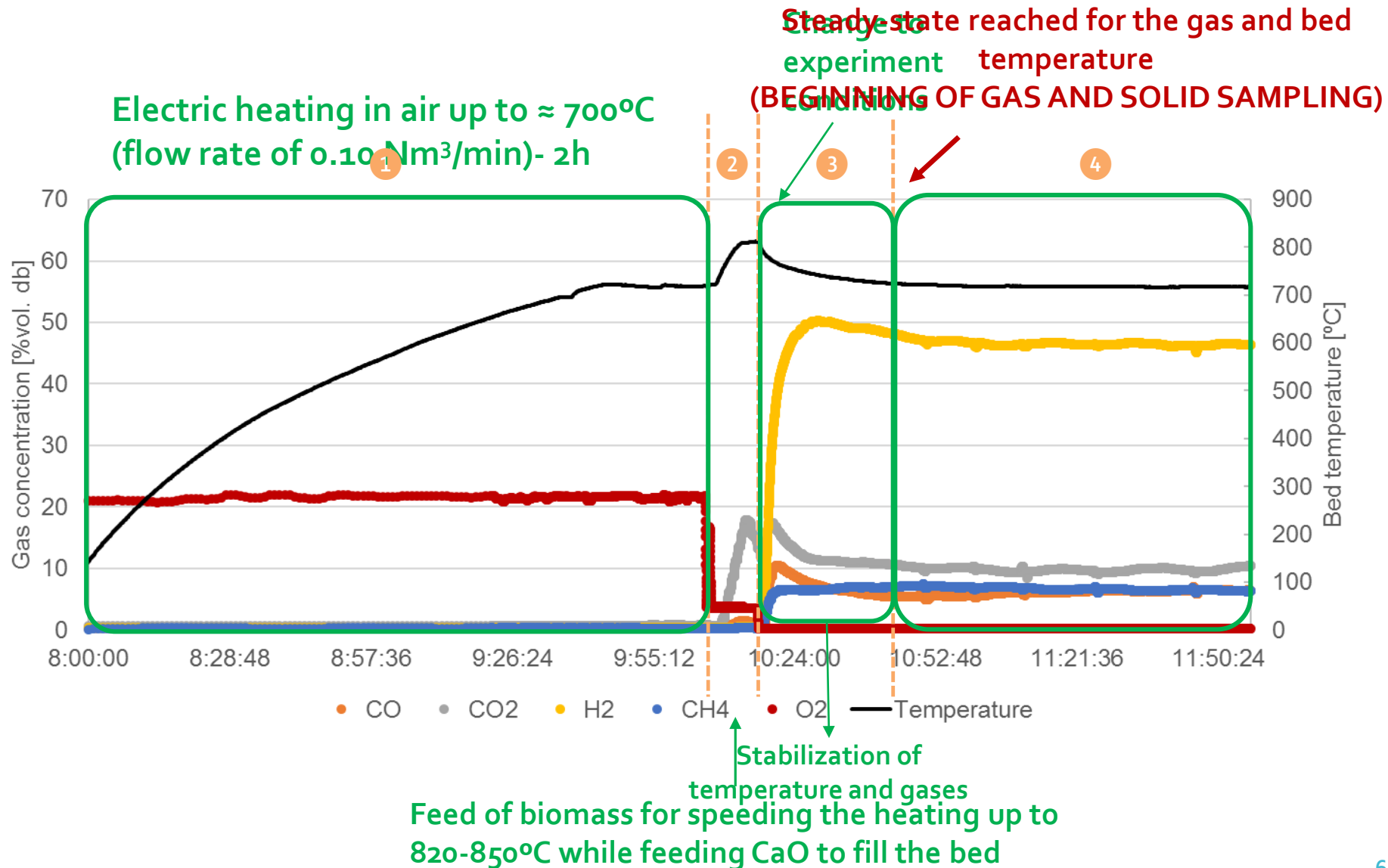
	Calcined limestone
CaO [%wt]	98.25
Al <sub>2</sub> O <sub>3</sub> [%wt]	0.145
Fe <sub>2</sub> O <sub>3</sub> [%wt]	0.002
K <sub>2</sub> O [%wt]	<0.001
MgO [%wt]	0.183
Na <sub>2</sub> O [%wt]	<0.001
SiO <sub>2</sub> [%wt]	0.132
Porosity [-]	0.52
Surface area [m <sup>2</sup> /g]	8.8
Solid density [kg/m <sup>3</sup> ]	3139



- High purity limestone
- Mean particle diameter: 450 microns
- Typical CO<sub>2</sub> sorption decay of natural Ca-based sorbents



- Bubbling Fluidized Bed (BFB) reactor
- 3 m height (Bottom part: 0.15 m x 1 m)
- Independent screw feeders
- Externally heated
- Bed inventory ≈ 5-6 kg (lateral overflow)
- N<sub>2</sub> flow rate fed to the evaporator (heater) and to the CaO screw feeder



S/C ratio \ Ca/C ratio	1	1.5
0.55	Green	Green
0.5	Green	White
0.45	White	Green
0.4	Green	White
0.3	White	Green

- Different Ca/C ratios (0.3-0.55) and S/C ratios (1 and 1.5) tested
- Stabilization temperature between 707 and 755°C
- Effect of CO<sub>2</sub> carrying capacity of the sorbent used tested

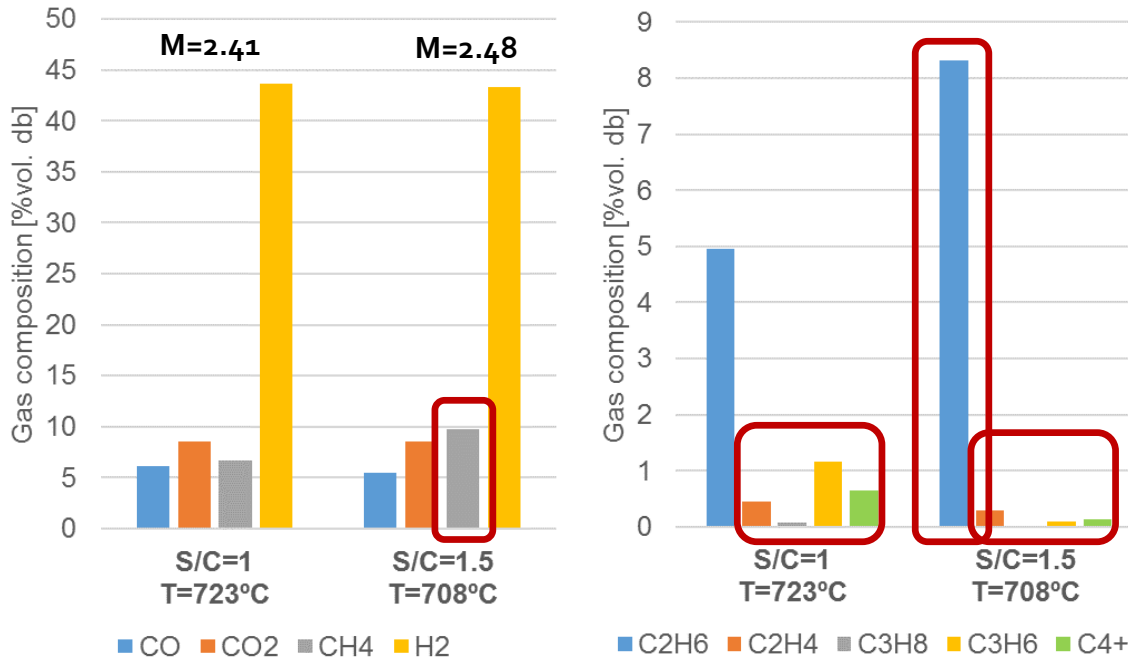
Char conversion in the BFB gasifier:

$$X_{CHAR} = 1 - \frac{m_{C,s \text{ overflow}}}{m_{FC,biomass}}$$

Char particles residence time:

$$\tau_{CHAR} = \frac{m_{char,SS}}{\dot{m}_{biomass} \cdot (y_{FC} + y_{ash})}$$

### ✓ Effect of S/C ratio (Ca/C ratio constant)



Ca/C ratio	0.53-0.55
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S/C	Gas yield (db) [Nm <sup>3</sup> /min]	X <sub>CHAR</sub> [%]	τ <sub>CHAR</sub> [min]
1	0.050	41-42	34
1.5	0.055	37	35

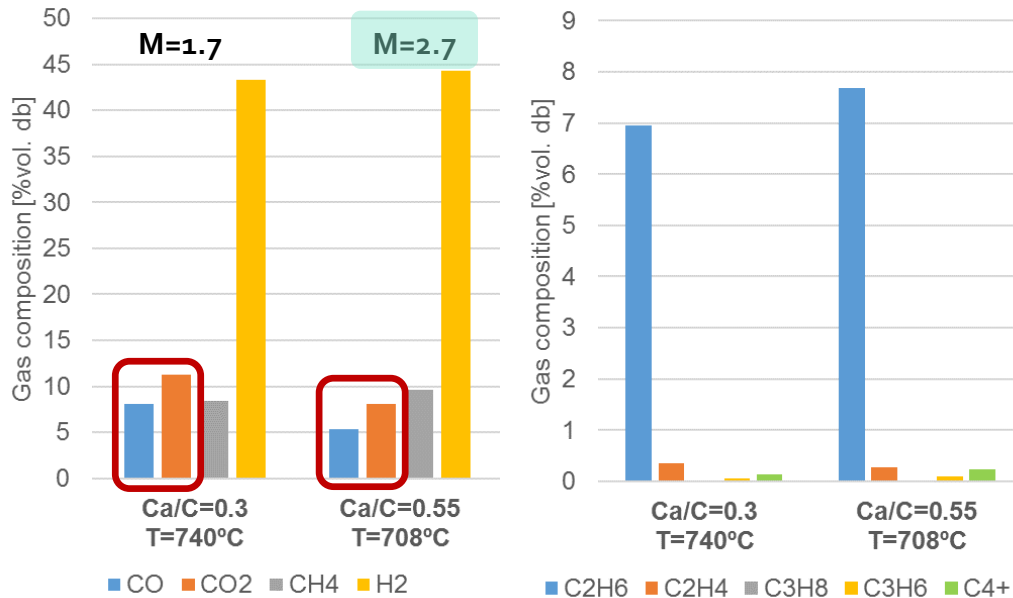
**M module:**

$$M = \frac{H_2 - CO_2}{CO + CO_2}$$

- Amount of C<sub>3</sub>+ and unsaturated C<sub>2</sub> reduced <0.53%vol. with S/C ratio of 1.5 (≈2.4%vol. for S/C=1)
- C<sub>3</sub>+ and C<sub>2</sub>H<sub>4</sub> cracked into C<sub>2</sub>H<sub>6</sub> and CH<sub>4</sub>, resulting into a larger gas yield
- Solid residence time for char particles has not changed, differences in conversion due to temperature



### ✓ Effect of Ca/C ratio (S/C ratio constant)



S/C ratio	1.5
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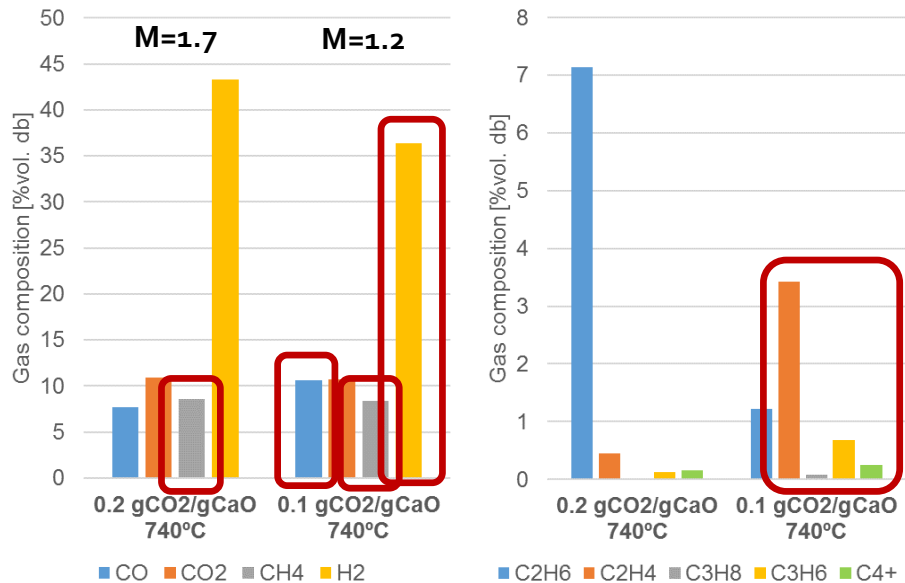
Ca/C	Gas yield (db) [Nm <sup>3</sup> /min]	X <sub>CHAR</sub> [%]	τ <sub>CHAR</sub> [min]	X <sub>CaO</sub> [%]
0.3	0.065	41	50	22-23
0.55	0.055	37	35	27

**M module:** 
$$M = \frac{H_2 - CO_2}{CO + CO_2}$$

- No effect on C<sub>3</sub>+ and unsaturated C<sub>2</sub> (<0.59%vol.) since S/C ratio is high
- CH<sub>4</sub> (and C<sub>2</sub>H<sub>6</sub>) is slightly higher for Ca/C=0.55 due to the lower stabilization temperature when Ca/C increases
- Larger M module for Ca/C=0.5 (lower temperature): linked to the amount of CO<sub>2</sub> separated
- Lower temperature and larger excess of CaO improve CO<sub>2</sub> separation and reduce CO<sub>2</sub> in the syngas (→ less CO content since WGS reaction is pushed)

### ✓ Effect of CO<sub>2</sub> sorbent activity (S/C and Ca/C ratios constant)

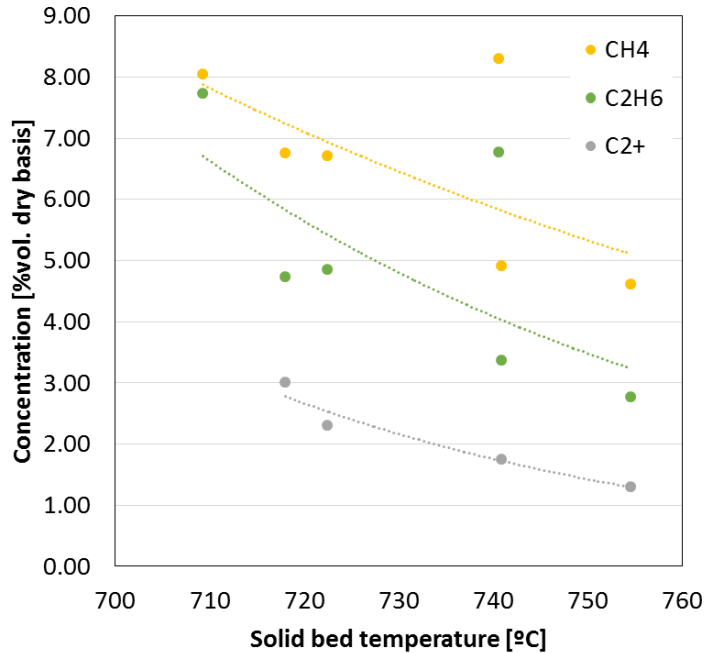
S/C ratio	1.5
Ca/C ratio	0.3



- Less CO<sub>2</sub> is separated from the gas phase (less activity of the CaO) → lower amount of H<sub>2</sub> and higher CO
- CH<sub>4</sub> concentration is kept constant at 8.5%vol. (db) (stabilization temperature is the same)
- Amount of C<sub>3</sub>+ and unsaturated C<sub>2</sub> increased for deactivated CaO (4.4%vol. vs 0.7%vol.) → less H<sub>2</sub> produced (less cracking into saturated C<sub>2</sub> and CH<sub>4</sub>)
- Increased gas yield for more active CO<sub>2</sub> sorbent since the amount of lighter C+ and H<sub>2</sub> is raised

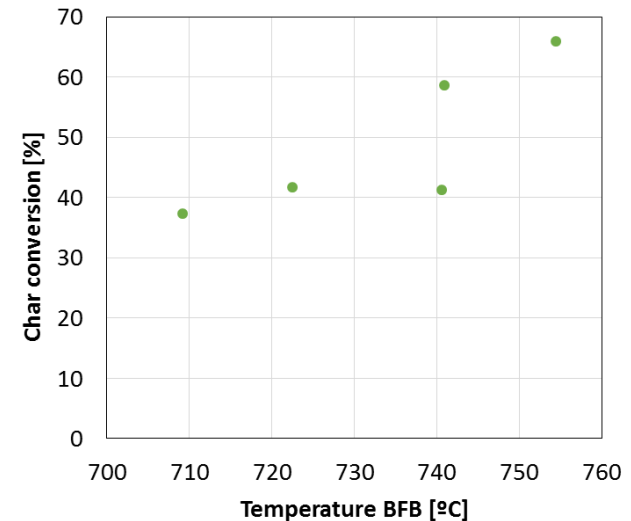
$g_{CO_2}/g_{CaO}$	Gas yield (db) [Nm <sup>3</sup> /min]	$X_{CHAR}$ [%]	$\tau_{CHAR}$ [min]	$X_{CaO}$ [%]
0.2	0.065	41	50	22-23
0.1	0.056	40	48	15

### ✓ Factors influencing the efficiency of the biomass-to-biofuel process



- Important to **reduce the CH<sub>4</sub> and C<sub>2+</sub> concentrations** (inerts → reduce yield and decrease the global efficiency)
- Dependence of HCs content on temperature → higher temperature decreases HCs concentration (except for C<sub>2+</sub> and S/C=1.5, not depicted in figure)
- Limit on HCs reduction → **need of conditioning steps** before the synthetic fuel production process (i.e. reforming stage)

- Char conversion in the gasifier influenced by the temperature (CaO excess and  $\tau$  barely affect)
- Efficiency of the SEG has an optimum: increasing char conversion boosts the efficiency but if there is not enough unconverted char in the combustor/calciner, additional biomass is needed (↓ efficiency)



- ✓ The **effect of the steam-to-carbon, CO<sub>2</sub> sorbent-to-biomass and the sorbent CO<sub>2</sub> carrying capacity** have been assessed for the sorption enhanced gasification of grape seeds
- ✓ S/C ratios of 1.5 needed for reducing C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>+ concentrations below 0.6%vol. (db), which will impact the downstream fuel production process
- ✓ CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> concentrations have shown dependence with temperature (i.e. decreases with increasing temperature). CH<sub>4</sub> contents as low as 4.5 %vol. (db) at around 755°C have been obtained
- ✓ A wide range of M modules has been obtained (M=1.7-2.7) , suitable for producing different types of biofuels (i.e., M=2 for DME or M=3 for SNG)

## FUTURE WORK

- ✓ Tar and S- compounds analysis to be tuned-up (analysis under different operating conditions in the next campaign)
- ✓ Higher S/C and wider range of temperatures to be tested
- ✓ Other biomasses to be studied

# Thanks for you attention

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