

› SORPTION ENHANCED DME SYNTHESIS FOR HIGH CARBON EFFICIENCIES

ECCE 12 | J. van Kampen

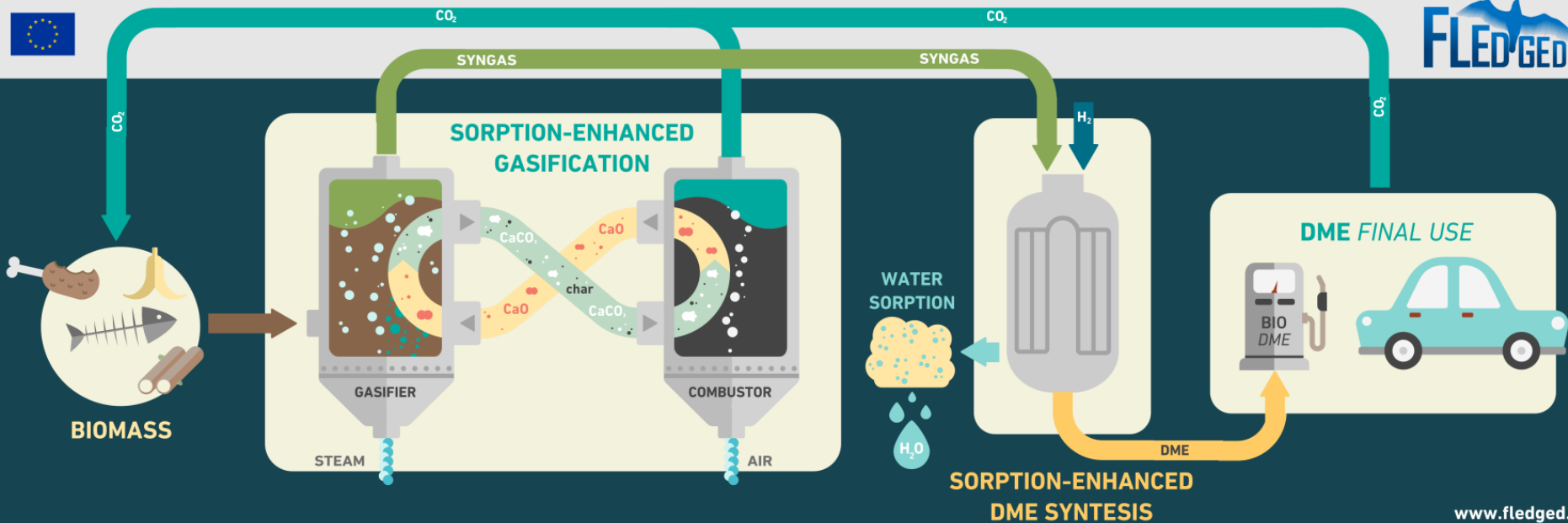
TU/e



ECN ›

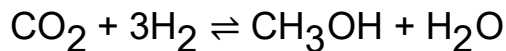
TNO

innovation
for life

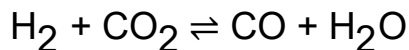


CONVENTIONAL DME SYNTHESIS

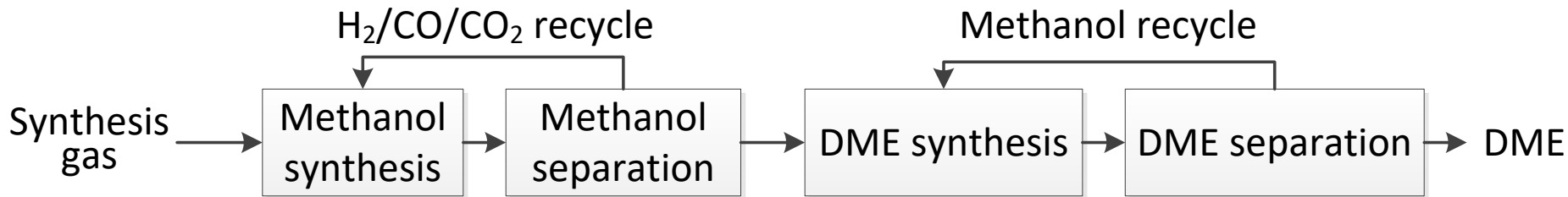
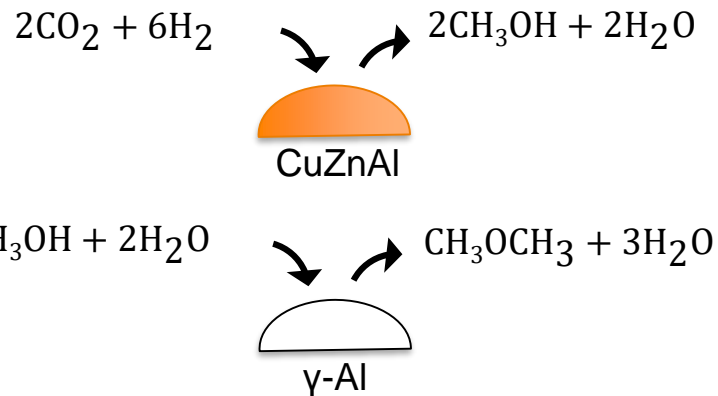
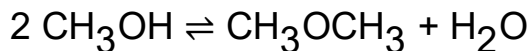
› Methanol synthesis:



› Reverse water-gas shift:

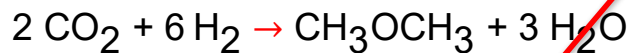


› Methanol dehydration:

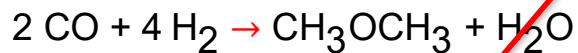


SORPTION ENHANCED DME SYNTHESIS (SEDMES)

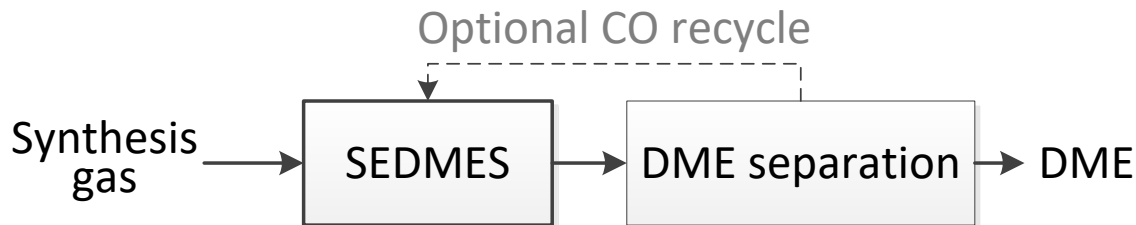
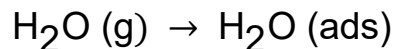
› Direct DME:



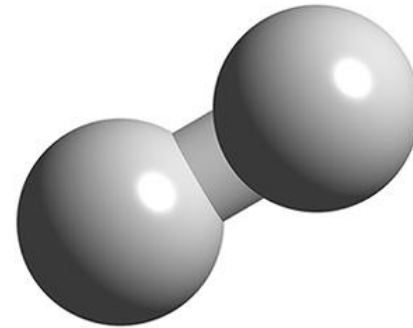
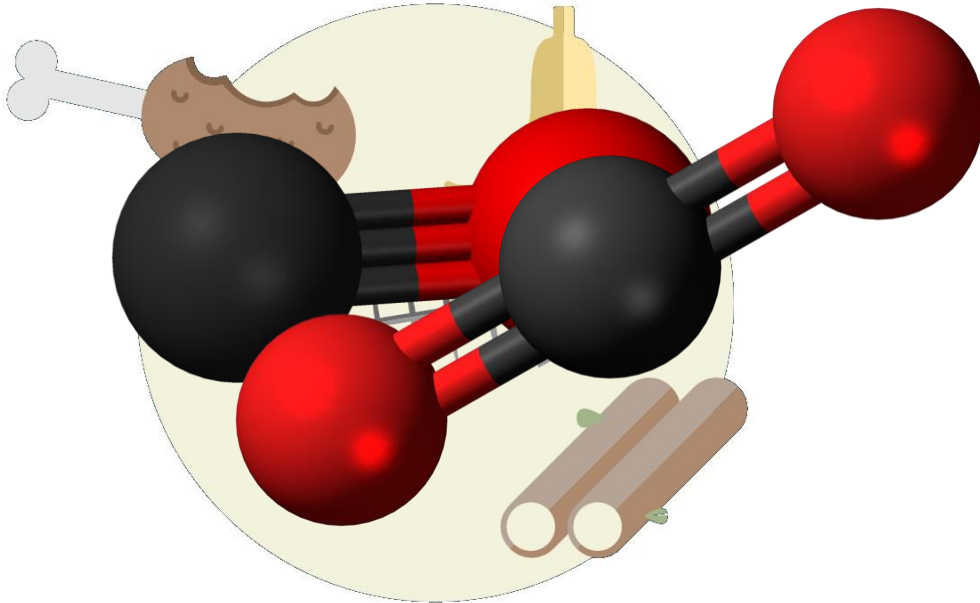
› Direct DME:



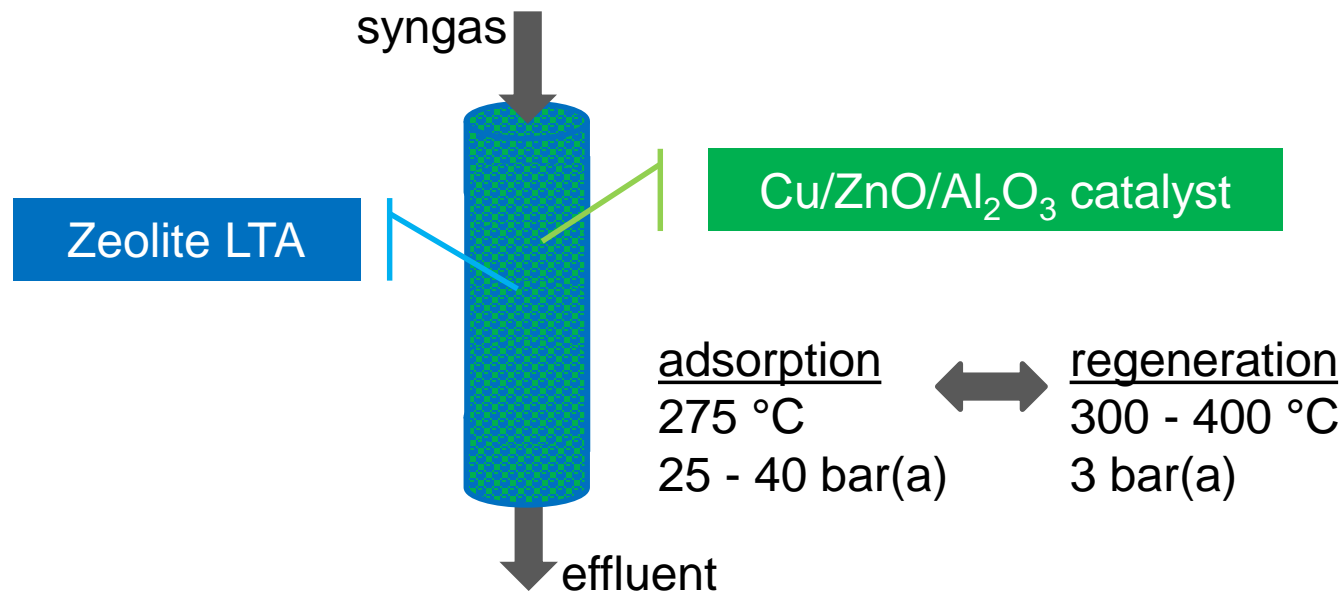
› Adsorption:



FEED FLEXIBILITY



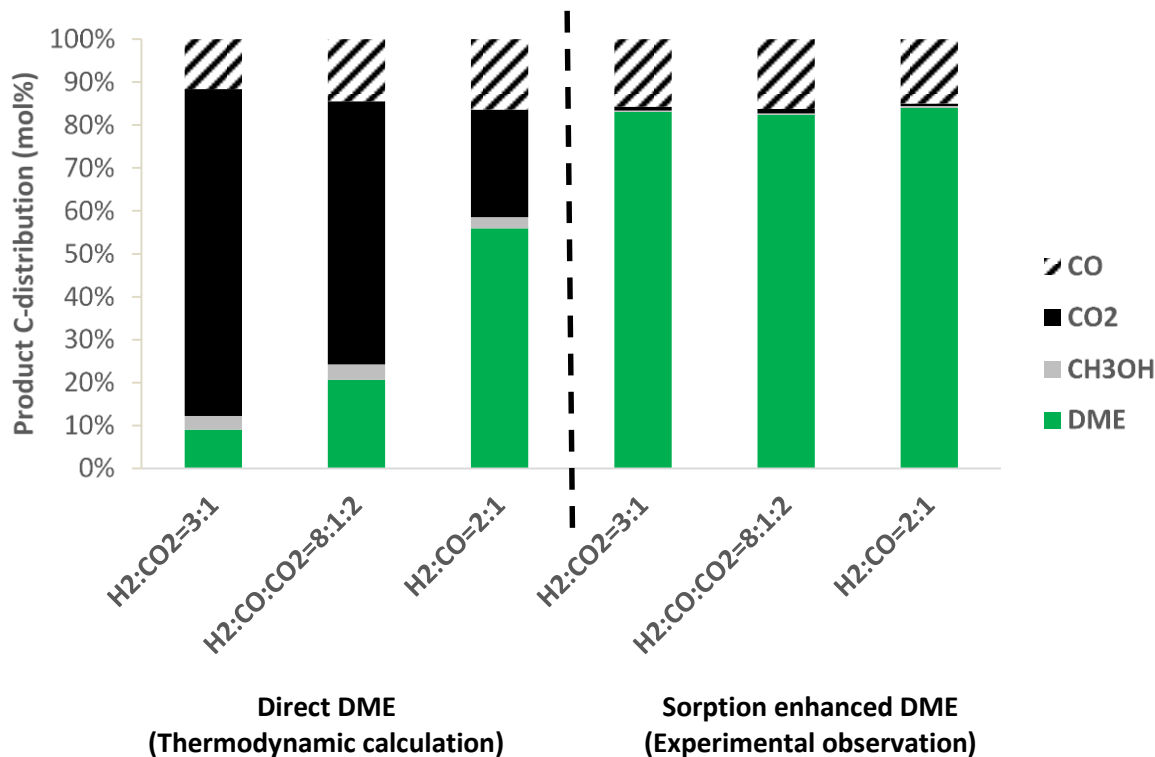
EXPERIMENTAL: SEDMES



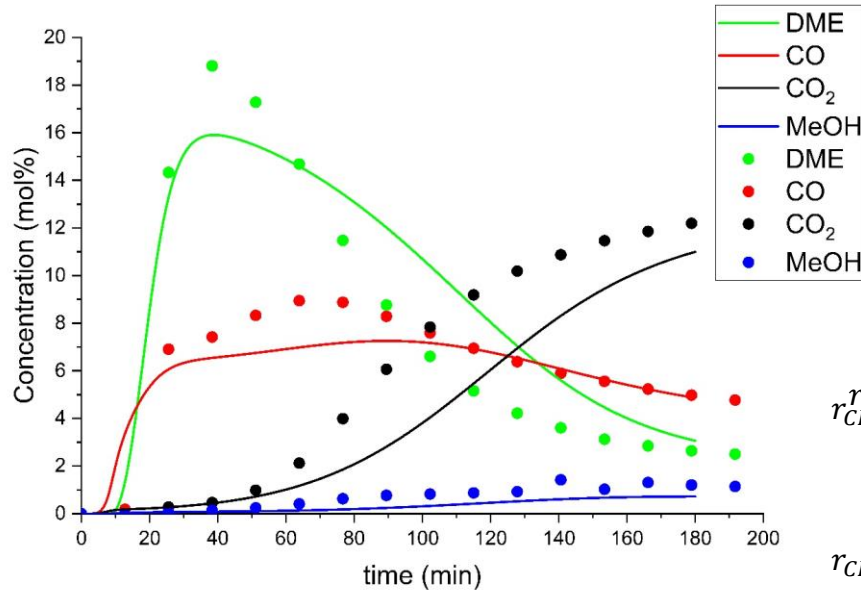
SEDMES FEED FLEXIBILITY

- › Direct DME synthesis
- › 275 °C & 40 bar(a), incl. 30% inert
- › Carbon is found in CO / CO₂ / MeOH / DME
- › Sorption enhanced DME synthesis
- › 275 °C & 40 bar(a), incl. 30% inert
- › Carbon is found in CO / CO₂ / ~~MeOH~~ / DME

van Kampen et al., Chemical Engineering Journal 374 (2019) 1286–1303.



SEDMES BREAKTHROUGH MODEL



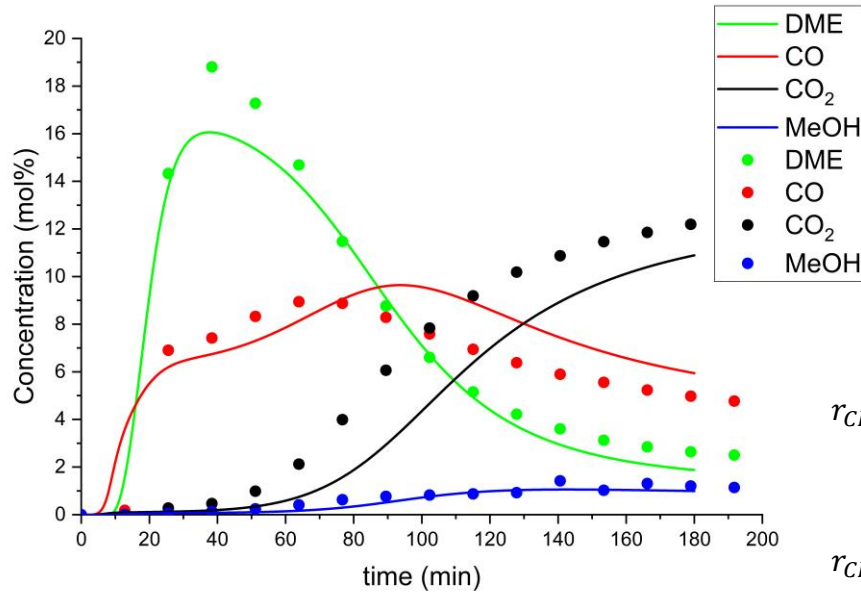
Canal et al., Chemical Engineering Science 46 (1991) 1889-195.

$$r_{CO} = r_{RWGS} = \frac{k'_{RWGS} K_{CO} \left[\frac{1}{\phi_{CO} \phi_{H_2}} \left(\frac{\phi_{H_2O} \phi_{H_2}}{K_{H_2O} \phi_{CO} \phi_{H_2}} \right) \right]}{(1 + K_{CO} \phi_{CO} + K_{CO_2} \phi_{CO_2}) \left[\phi_{H_2}^{1/2} \sqrt{K_{H_2O} \phi_{H_2O} + K_{H_2}^{1/2} \phi_{H_2O}} \right]}$$

$$r_{CH_3OH,1} = \frac{k'_{CH_3OH,1} K_{CO} \left[\frac{1}{\phi_{CO} \phi_{H_2}} \left(\frac{\phi_{CH_3OH} \phi_{H_2}}{K_{CH_3OH} \phi_{CO} \phi_{H_2}} \right) \right]}{(1 + K_{CO} \phi_{CO} + K_{CO_2} \phi_{CO_2}) \left[\phi_{H_2}^{1/2} \sqrt{K_{H_2O} \phi_{H_2O} + K_{H_2}^{1/2} \phi_{H_2O}} \right]}$$

$$r_{CH_3OH,2} = \frac{k_3 K_{CO_2} \left[\phi_{CO_2} \phi_{H_2}^{3/2} - \phi_{CH_3OH} \phi_{H_2O} / (\phi_{H_2}^{3/2} K_{p3}) \right]}{(1 + K_{CO} \phi_{CO} + K_{CO_2} \phi_{CO_2}) \left[\phi_{H_2}^{1/2} + (K_{H_2O} / K_{H_2}^{1/2}) \phi_{H_2O} \right]}$$

SEDMES BREAKTHROUGH MODEL



Graaf et al., Chemical Engineering Science 43 (1988) 3185-3195.

$$r_{CO} = \frac{k_2 K_{CO2} [\varphi_{CO2} \varphi_{H2} - \varphi_{H2O} \varphi_{CO} / K_{p2}]}{(1 + K_{CO} \varphi_{CO} + K_{CO2} \varphi_{CO2}) [\varphi_{H2}^{1/2} + (K_{H2O} / K_{H2}^{1/2}) \varphi_{H2O}]}$$

$$r_{CH3OH,1} = \frac{k_1 K_{CO} [\varphi_{CO} \varphi_{H2}^{3/2} - \varphi_{CH3OH} / (\varphi_{H2}^{1/2} K_{p1})]}{(1 + K_{CO} \varphi_{CO} + K_{CO2} \varphi_{CO2}) [\varphi_{H2}^{1/2} + (K_{H2O} / K_{H2}^{1/2}) \varphi_{H2O}]}$$

$$r_{CH3OH,2} = \frac{k_3 K_{CO2} [\varphi_{CO2} \varphi_{H2}^{3/2} - \varphi_{CH3OH} \varphi_{H2O} / (\varphi_{H2}^{3/2} K_{p3})]}{(1 + K_{CO} \varphi_{CO} + K_{CO2} \varphi_{CO2}) [\varphi_{H2}^{1/2} + (K_{H2O} / K_{H2}^{1/2}) \varphi_{H2O}]}$$

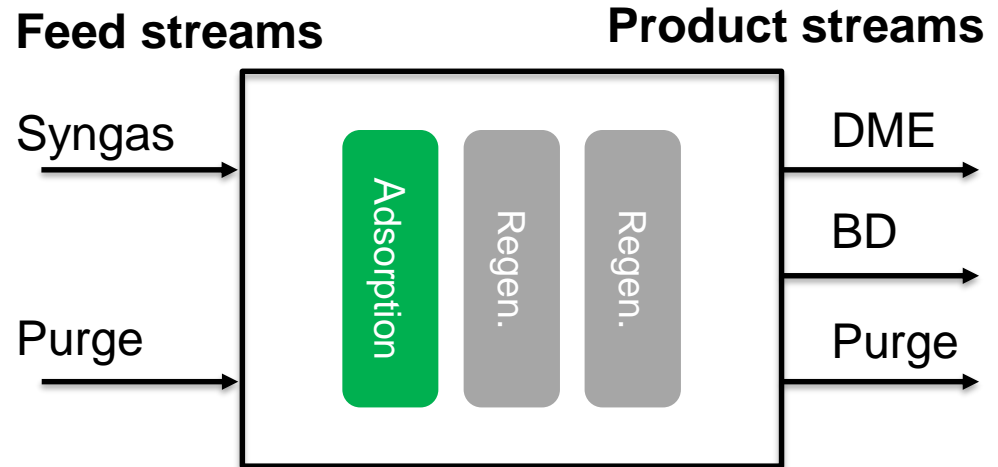
CYCLE DESIGN

- › 3 column continuous process
- › 4 step TPSA cycle:
 - › Adsorption
 - › Depressurization (Blowdown)
 - › Purge
 - › Repressurization

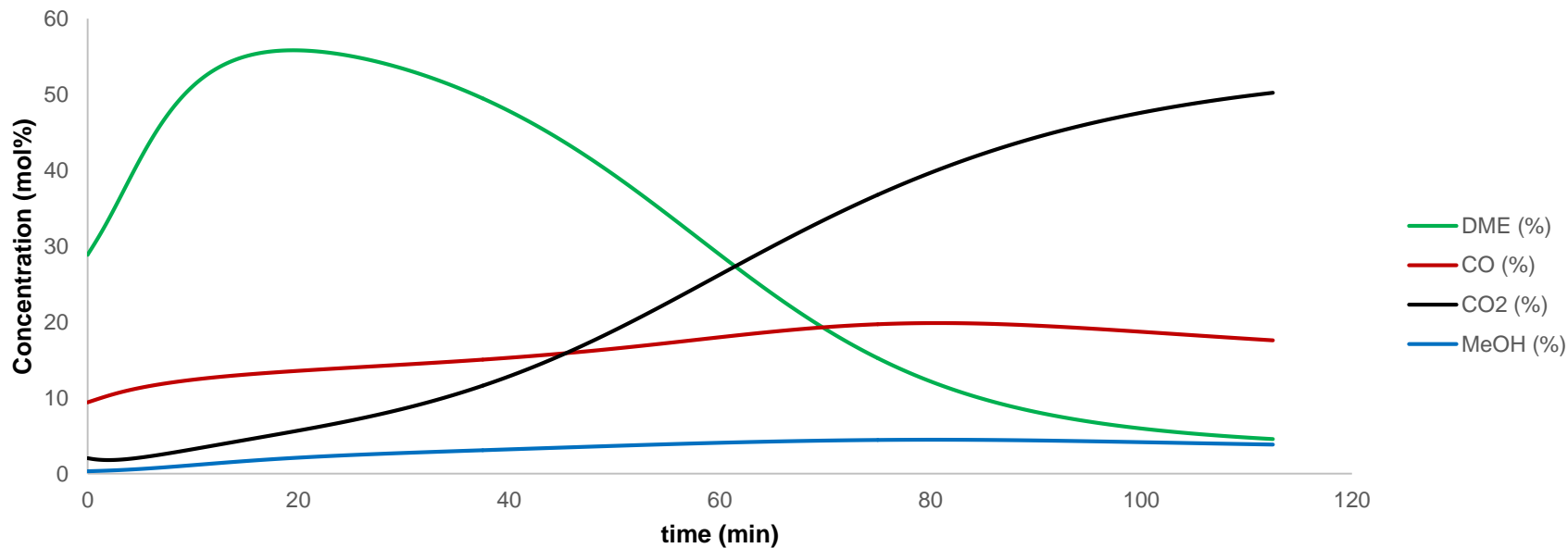


CYCLE DESIGN

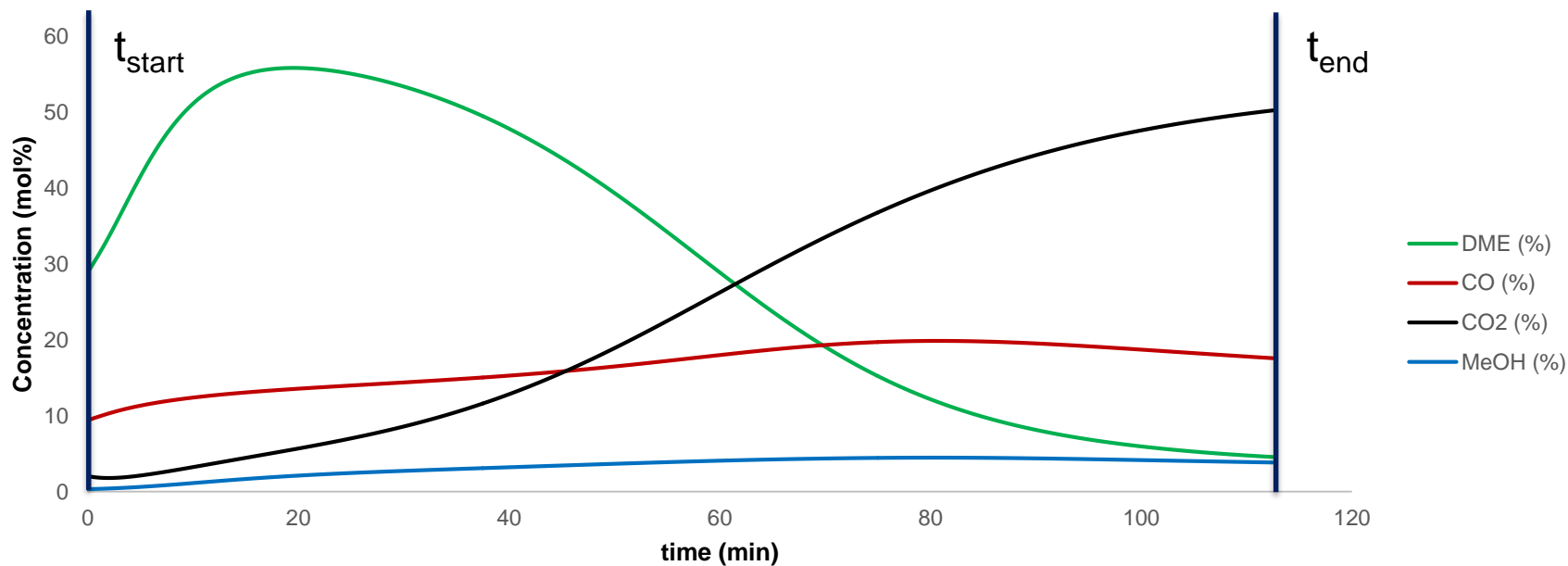
- › **3 column** design for continuous operation
- › 2 feed streams
 - › Syngas
 - › Purge gas
- › 3 product streams
 - › DME product
 - › Blowdown product
 - › Purge product



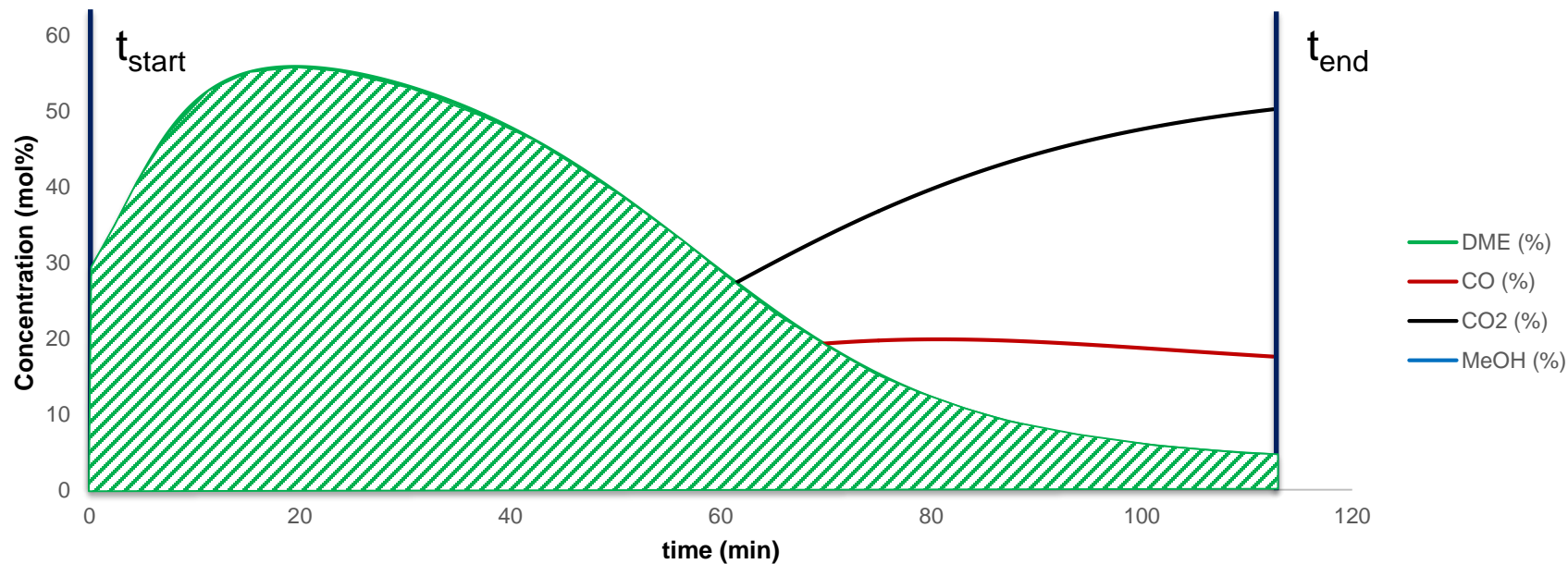
BASE CASE



BASE CASE



BASE CASE



FEED & PRODUCT

› Feed

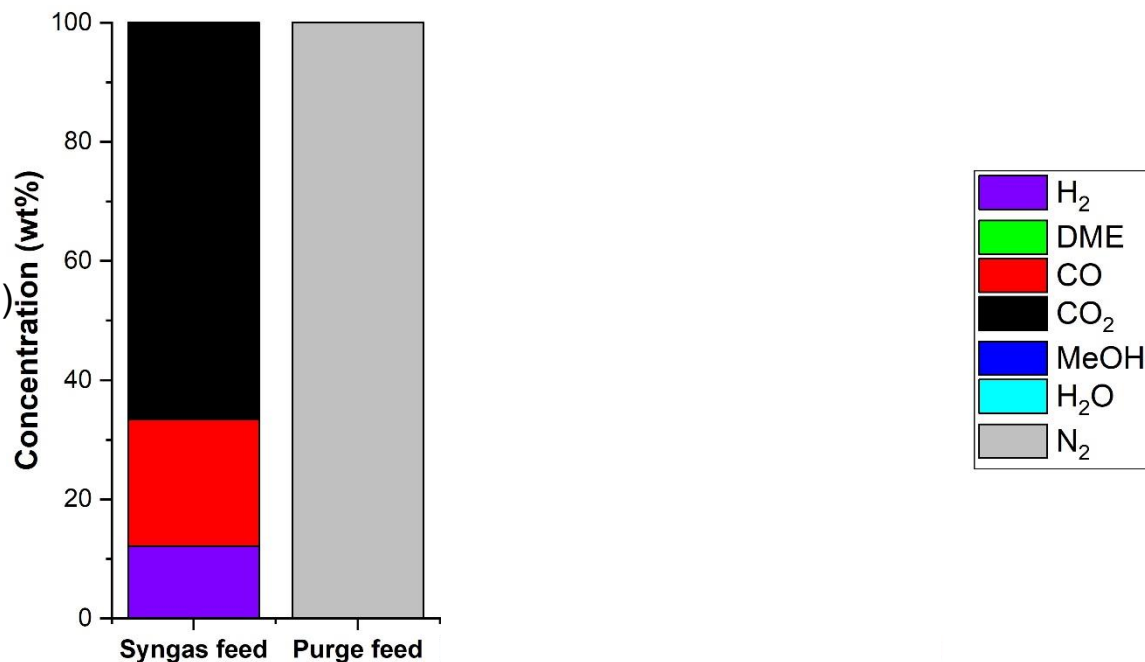
- › $\text{CO}_2:\text{CO}=2:1$
- › $M=2$

› Product

- › 64% conversion (unoptimized)
- › Thermodynamically only 26%

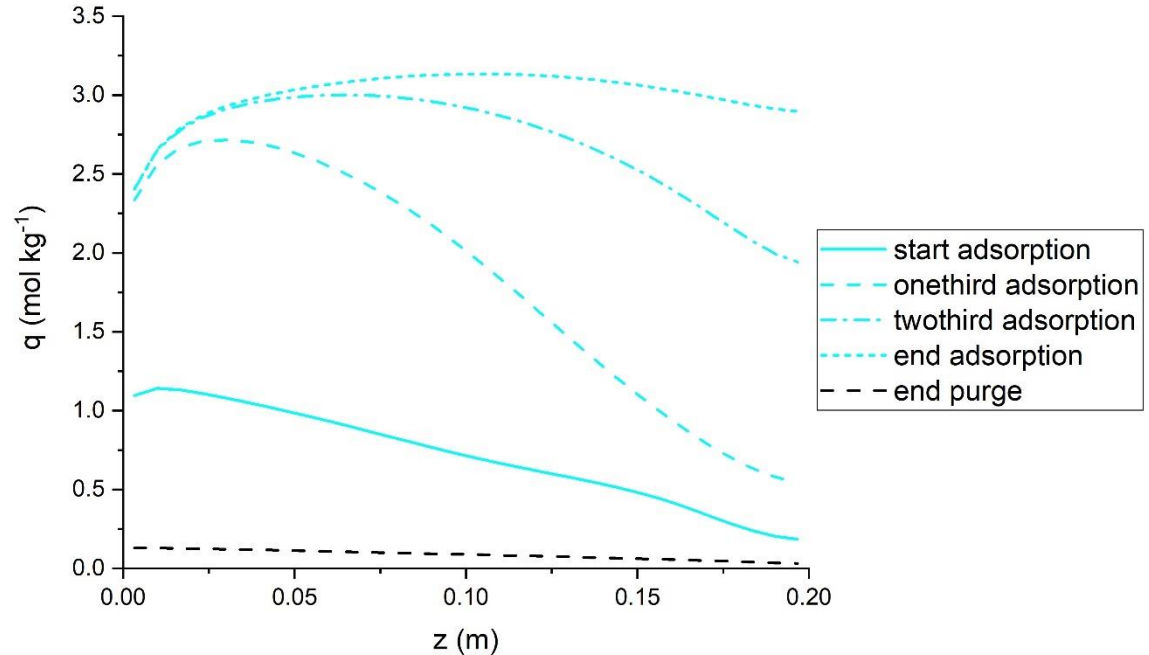
› Purge product: $\text{N}_2+\text{H}_2\text{O}$

- › recycle



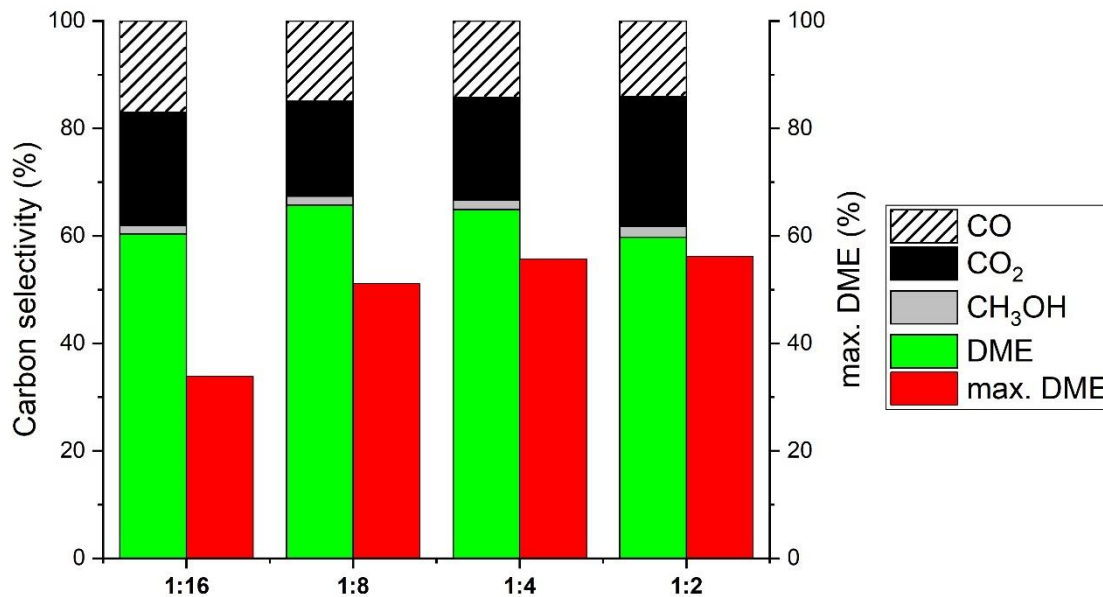
WORKING CAPACITY

- › Working capacity
 - › adsorption
 - › regeneration
- › Determines conversion & yield
 - › Limitation
- › Depends on
 - › Process conditions
 - › **Regeneration**



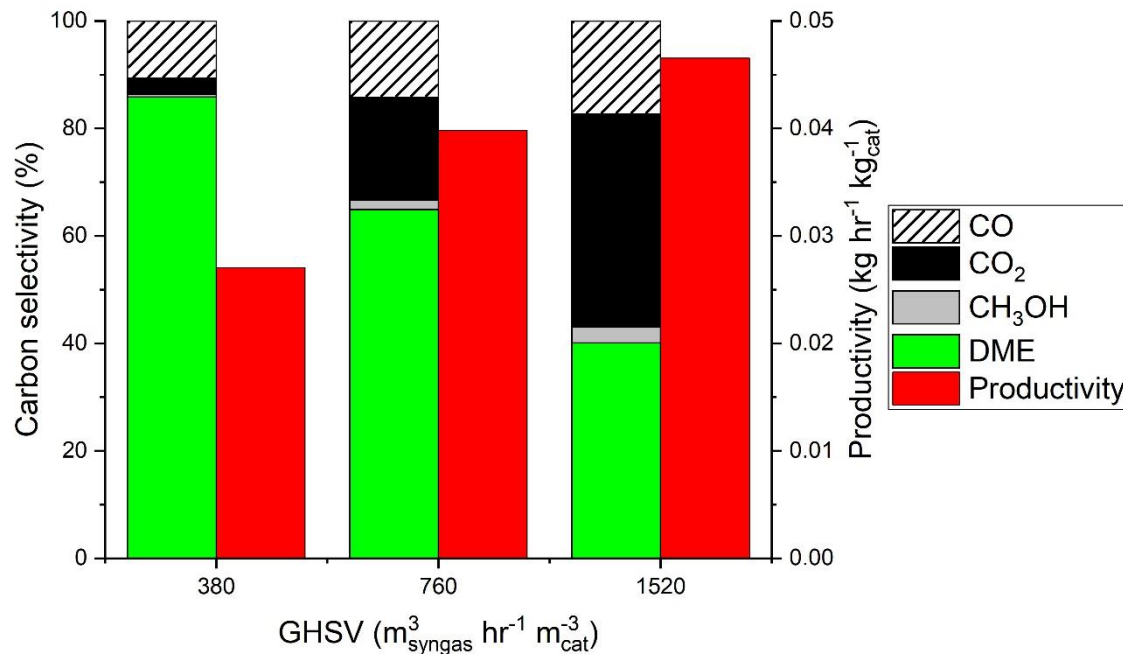
CATALYST VS. SORBENT

- › Working capacity limited
- › Increasing adsorbent beneficial
 - › Penalty reducing catalyst



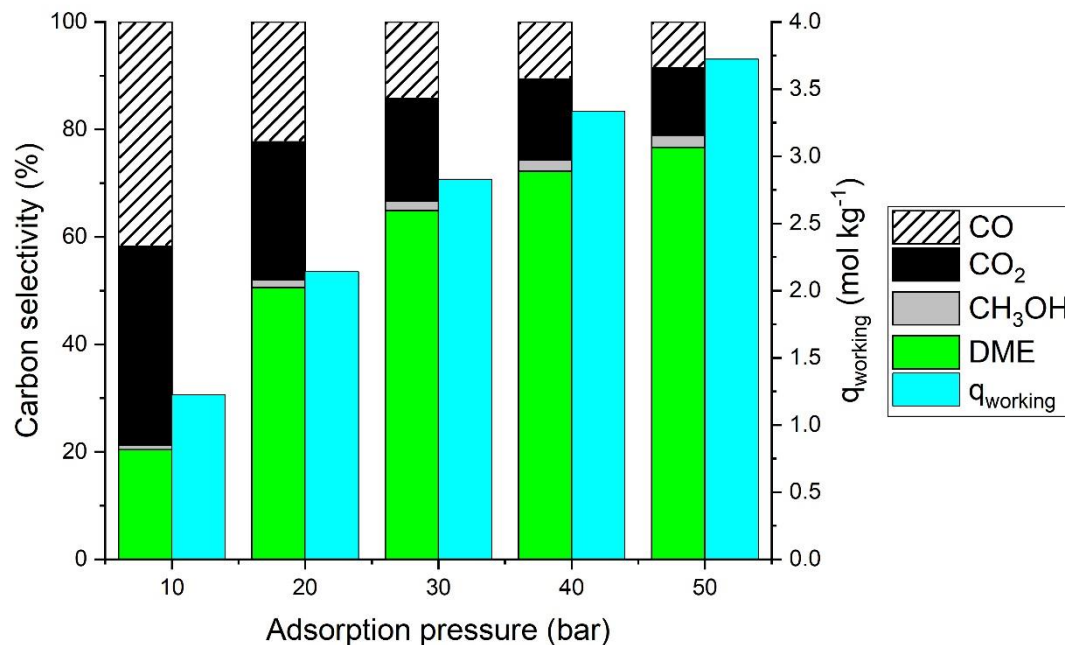
SELECTIVITY VS. PRODUCTIVITY

- › Lower GHSV, lower steam content
- › Trade-off
 - › Higher conversion & selectivity
 - › Lower productivity



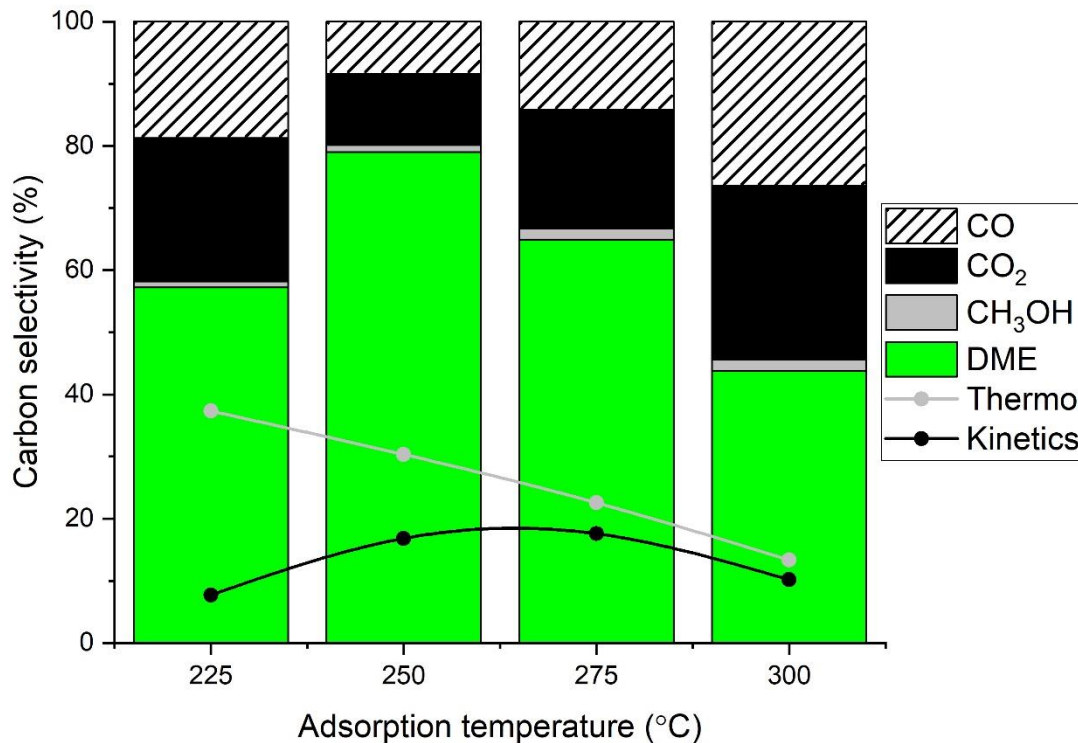
PRESSURE

- › Pressure
 - › Increased methanol synthesis
 - › Increased working capacity
- › Flowsheet optimisation



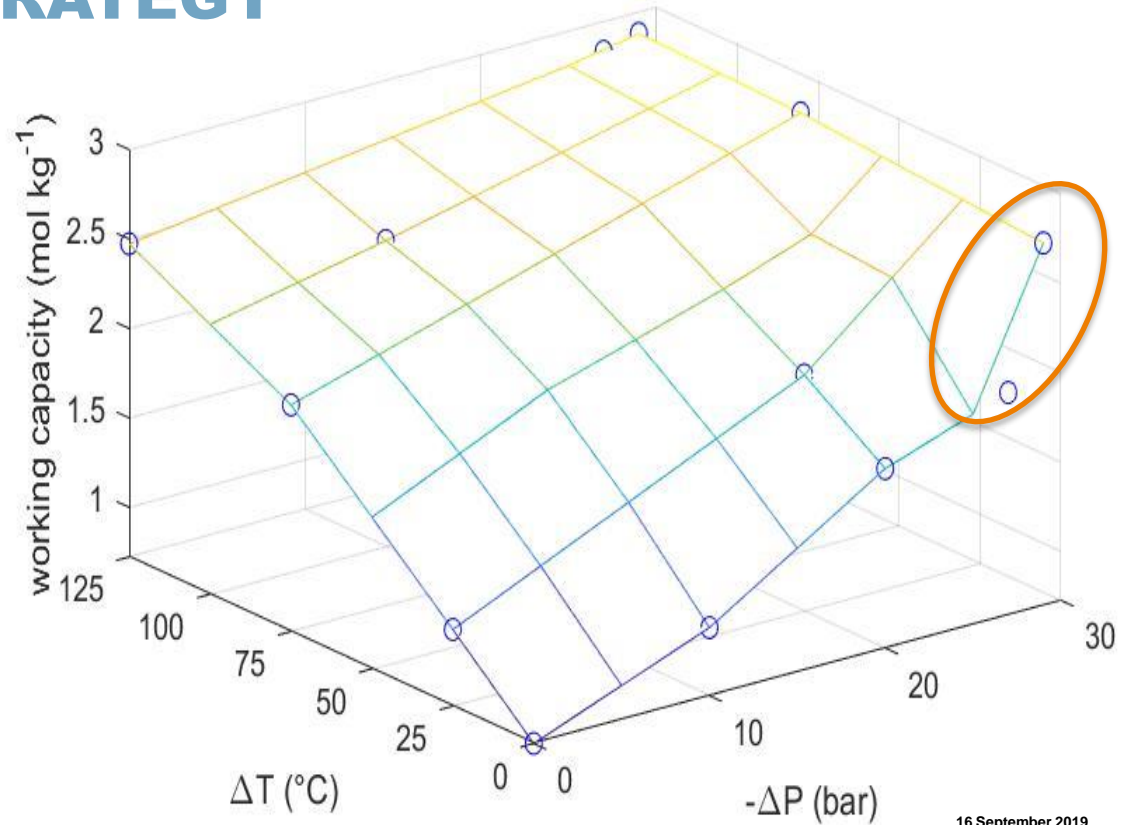
TEMPERATURE

- › Temperature
 - › Catalyst
 - › Activity vs. Thermo
 - › Adsorbent
 - › Isotherm capacity



REGENERATION STRATEGY

- › Temperature swing
- › Pressure swing
 - › Faster cycling
 - › Higher productivity
- › Window for PSA?



CONCLUSION

- › Sorption enhanced DME synthesis (SEDMES):
 - › Proof-of-concept
 - › High DME yield
 - › Feed flexibility → direct CO₂ utilisation

- › 3 column cycle design (TPSA)
- › Temperature swing regeneration to 400 °C
 - › Improves DME yield pre and post steam breakthrough
 - › Adsorbent capacity increases
- › Window for pressure swing regeneration?
 - › Increased productivity

OUTLOOK

- › Sorption enhanced DME synthesis (SEDMES):
 - › Regeneration strategy
 - › TSA vs PSA
 - › Heat management
 - › Adiabatic or non-adiabatic operation
 - › Integration of temperature swing regeneration
- › Scale-up & system design



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THANK YOU FOR YOUR ATTENTION



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https://youtu.be/JEn39Zi_aCg

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FLEXIBLE DIMETHYL ETHER PRODUCTION FROM BIOMASS GASIFICATION WITH SORPTION ENHANCED PROCESSES

