

# FLEDGED

## SORPTION-ENHANCED DIMETHYL ETHER SYNTHESIS (SEDMES)



**TNO**

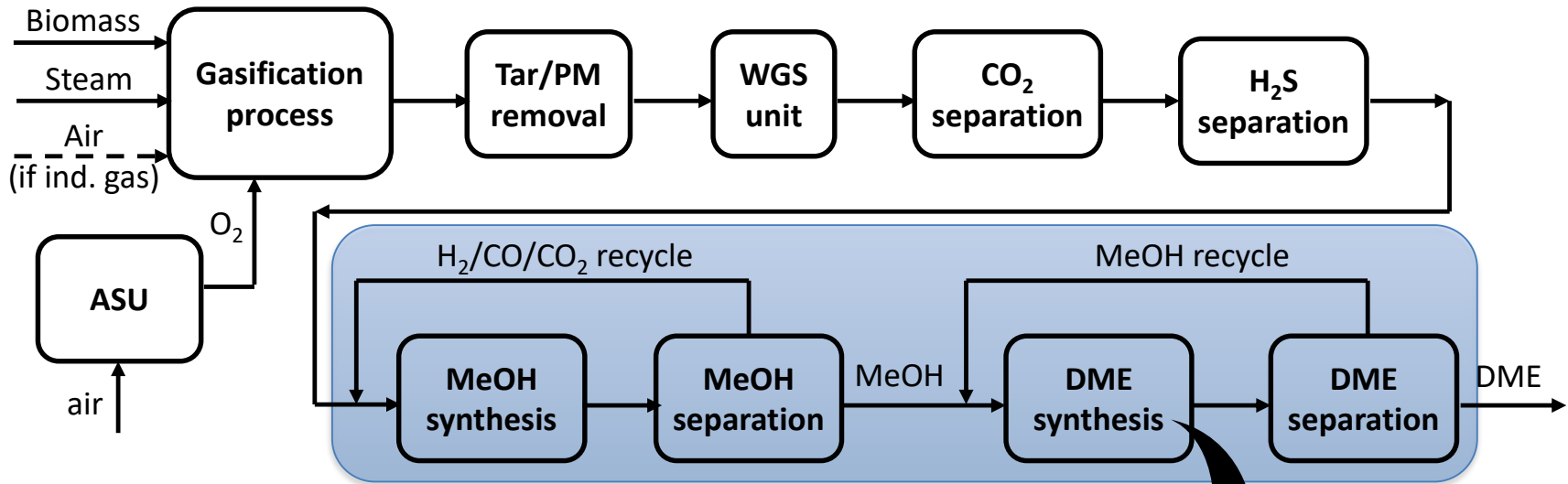
Laboratory  
of Catalysis and  
Catalytic Processes **LCCP**



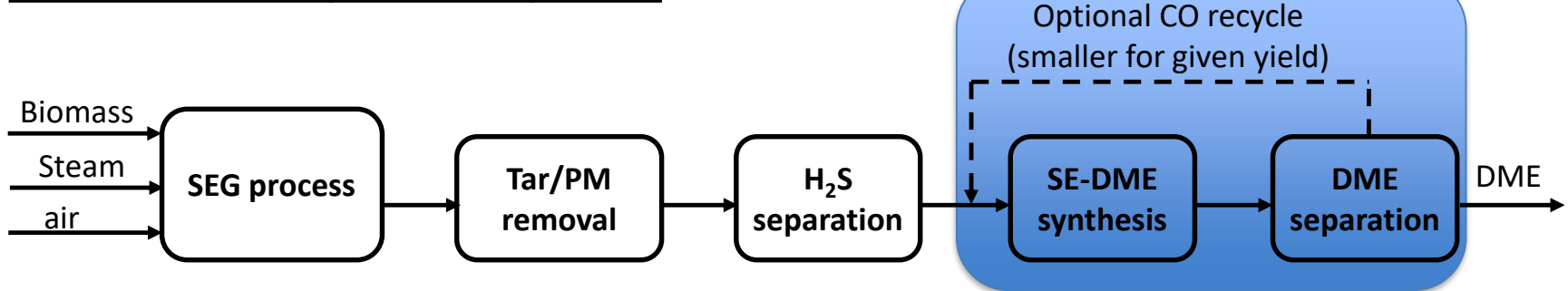
**POLITECNICO  
MILANO 1863**

# Process intensification: Sorption-Enhanced DME Synthesis

## Biomass to DME with conventional process



## Biomass to DME by FLEDGED process

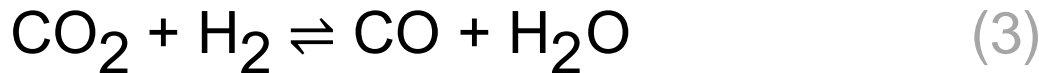
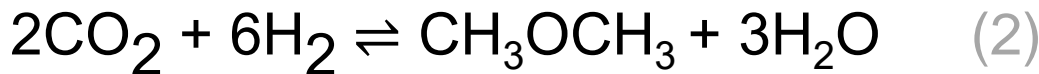


# Process intensification: Direct DME Synthesis

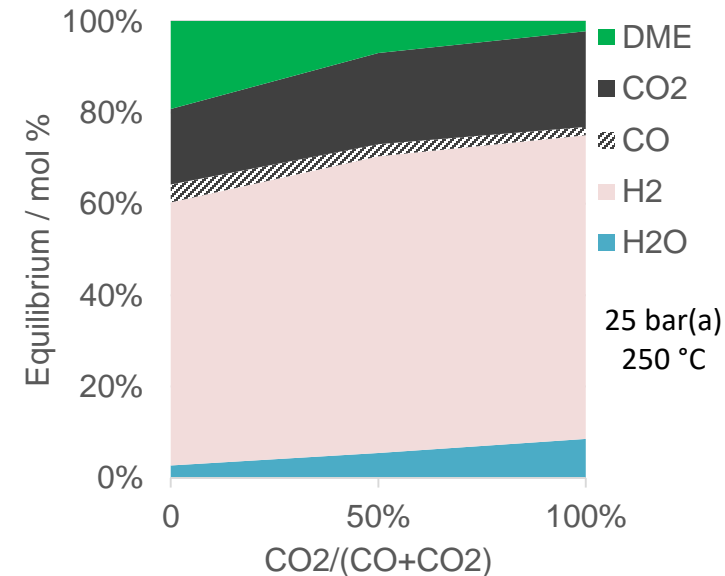
## Feed gas

CO and CO<sub>2</sub> with stoichiometric H<sub>2</sub> ( $M = \frac{[H_2] - [CO_2]}{[CO] + [CO_2]} = 2$ )

## Direct DME synthesis equilibrium



- Poor conversion per pass
- High CO<sub>2</sub> concentration product  
( $CO + H_2O \rightarrow CO_2 + H_2$ )



**TNO**

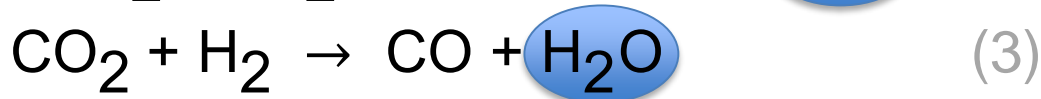
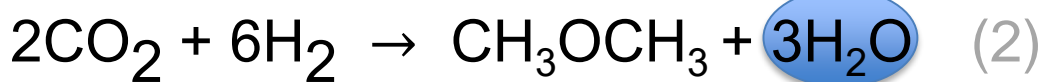
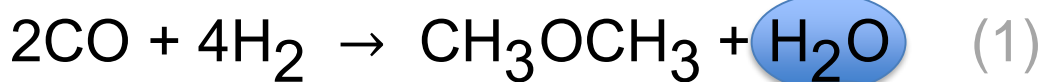
**FLEDGED**

# Process intensification: Sorption-Enhanced DME Synthesis

## Feed gas

CO and CO<sub>2</sub> with stoichiometric H<sub>2</sub> ( $M = \frac{[H_2] - [CO_2]}{[CO] + [CO_2]} = 2$ )

## Sorption-enhanced DME synthesis



- High conversion per pass
- High CO concentration product (CO<sub>2</sub> + H<sub>2</sub> → CO + H<sub>2</sub>O)



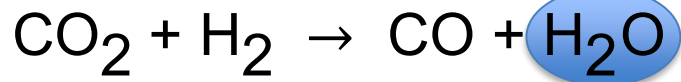
Henry Louis Le Chatelier (1850 – 1936)

# Process intensification: Sorption-Enhanced DME Synthesis

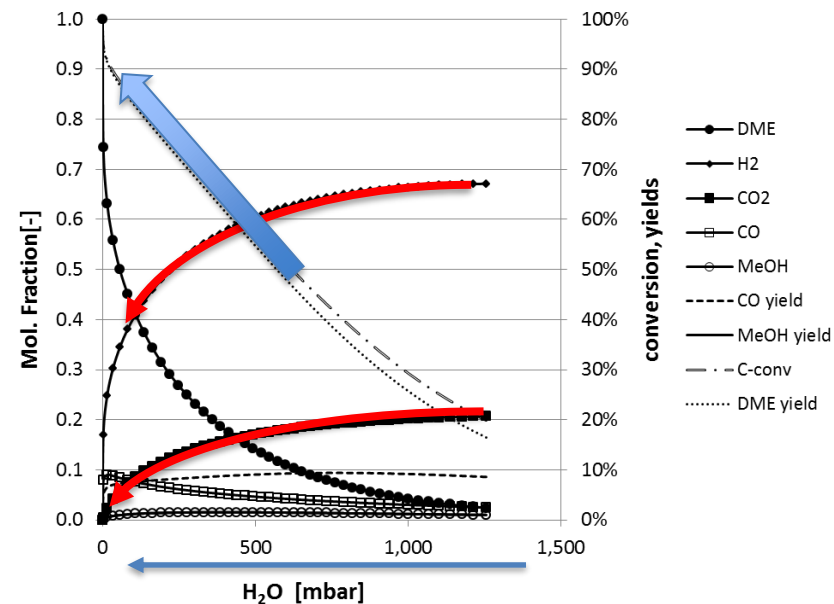
## Feed gas

CO and CO<sub>2</sub> with stoichiometric H<sub>2</sub> ( $M = \frac{[H_2] - [CO_2]}{[CO] + [CO_2]} = 2$ )

## Sorption-enhanced DME synthesis

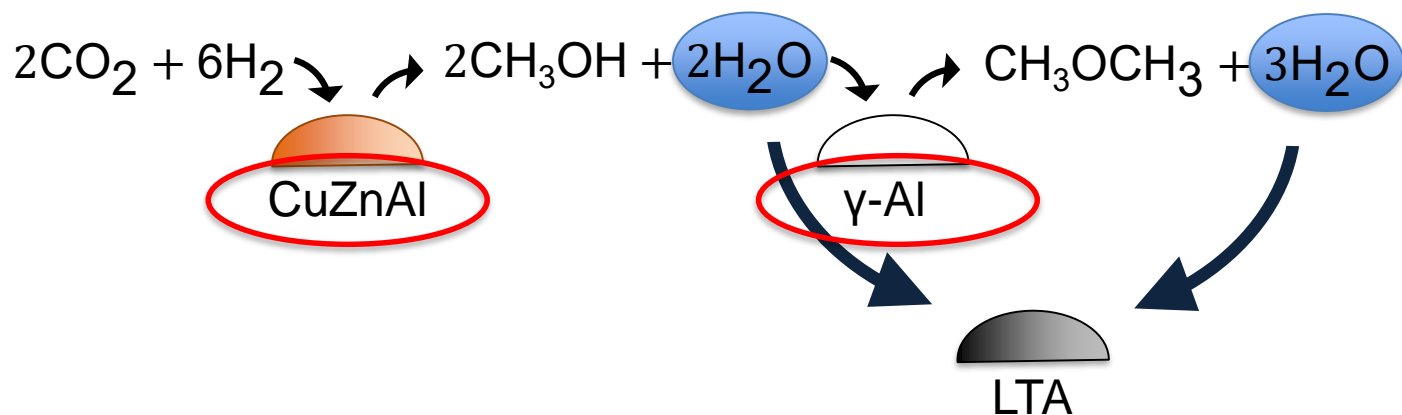


- High conversion per pass
- High CO concentration product (CO<sub>2</sub> + H<sub>2</sub> → CO + H<sub>2</sub>O)



# SEDMES

In sorption-enhanced DME synthesis, SEDMES, the equilibrium of direct DME synthesis is shifted by using a physical adsorbent



# Catalyst development

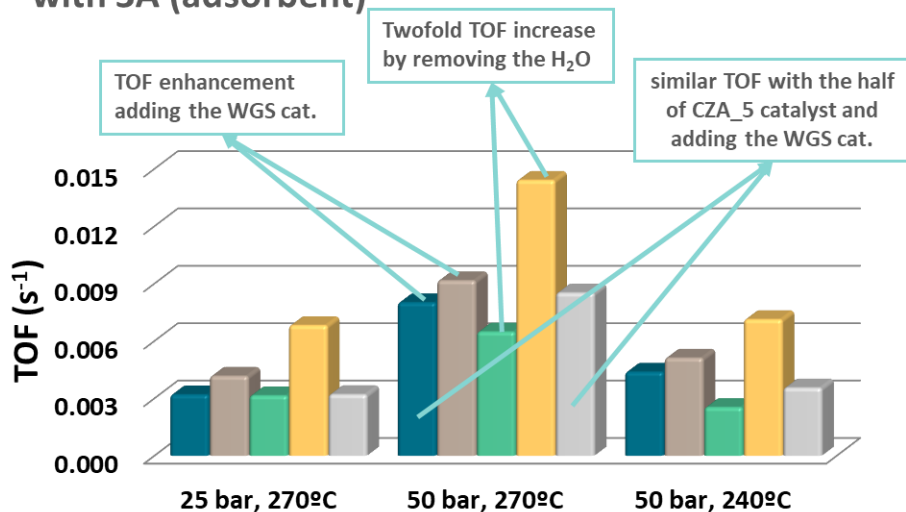
- Syngas → Methanol (CSIC made Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>, CZA)
  - Effect of CuO loading:  $> X_{CO+CO_2}$  at higher CuO loading (62 – 58 – 52 – 46 – 39 – 33 wt.%)
  - Effect of the syngas composition:  $> X_{CO+CO_2}$  at lower CO<sub>2</sub> content (CO<sub>2</sub>/CO= 1.9 and 1)
  - Effect of promoters: *no promotion effect of Zr, Ga or Pd*
  - Comparison with commercial catalyst Katalco<sup>TM</sup>51-8: *novel catalyst 62 wt.% CuO loading reached similar TOF*
- Methanol → DME (supported heteropolyacids, H<sub>4</sub>SiW<sub>12</sub>O<sub>40</sub> or H<sub>3</sub>PW<sub>12</sub>O<sub>40</sub>)
  - Effect of reaction conditions:  $> X_{MeOH}$  favoured at 180<T<240 °C and P> 24 bar
  - Effect of HPA nature:  $> X_{MeOH}$  with HSiW
  - Effect of the support:  $X_{MeOH}$ : SiO<sub>2</sub>>TiO<sub>2</sub>>ZrO<sub>2</sub>
  - Comparison with commercial catalysts: γ-Al<sub>2</sub>O<sub>3</sub> and HZSM-5
    - HZSM-5: *not selective for DME*
    - γ-Al<sub>2</sub>O<sub>3</sub>:  $X_{MeOH}$  with HSiW/SiO<sub>2</sub> or HSiW/TiO<sub>2</sub> thrice that with γ-Al<sub>2</sub>O<sub>3</sub>
- Characterization:

XRD, XPS, N<sub>2</sub> adsorption-desorption isotherms, H<sub>2</sub>-TPR, H<sub>2</sub>-N<sub>2</sub> and Air-TGA, SEM/EDX, TEM-STEM, NH<sub>3</sub>-TPD, N<sub>2</sub>O-Chemisorption, ICP-OES, NMR and Raman spectroscopy, at the ICP-CSIC. Some of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts were analysed by X-ray Absorption Spectroscopy at the ESRF synchrotron facilities in Grenoble (France)



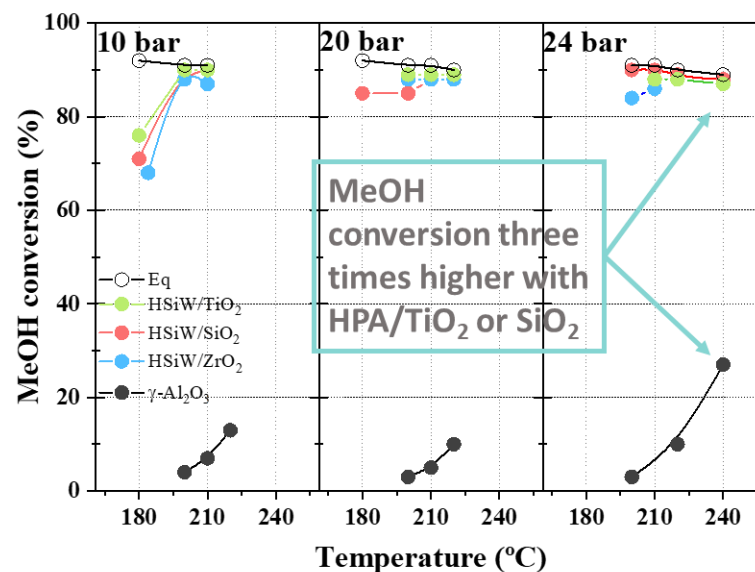
# Methanol synthesis & dehydration catalysis

- Methanol productivity enhancement: Double beds WGS (CZA\_50) & Methanol (CZA\_5) catalysts with 3A (adsorbent)



- CZA\_5 (7500 mLsyngas/h/mL CZA\_5)
- CZA\_50:CZA\_5= 1:1 (3750 mLsyngas/h/mL CZA\_5+CZA\_50)
- CZA\_50:CZA\_5= 2:1 (2500 mLsyngas/h/mL CZA\_5+CZA\_50)
- CZA\_50:CZA\_5= 2:1 + 3A (2500 mLsyngas/h/mL CZA\_5+CZA\_50)
- CZA\_50:CZA\_5= 1:1 (7500 mLsyngas/h/mL CZA\_5+CZA\_50)

- Low Temperature DME production from MeOH with novel catalysts



Stable methanol conversions (maintained at least for 6 h) for the HSiW/X catalysts and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> at different conditions of P and T



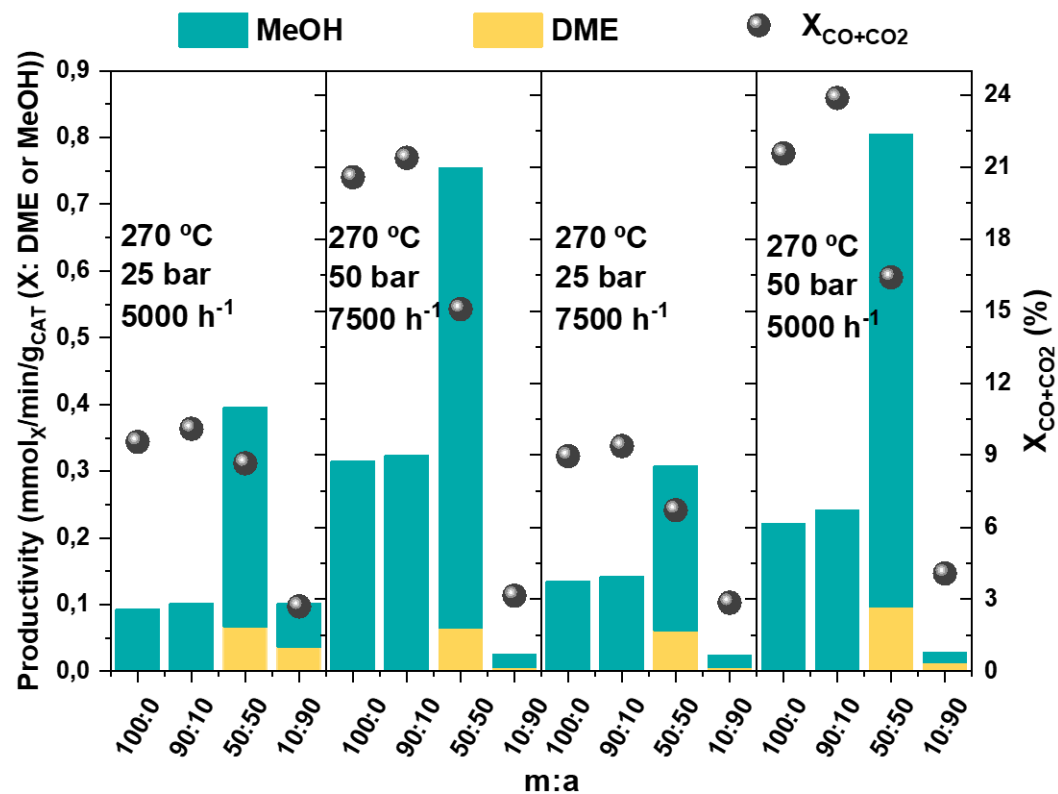


# Direct DME synthesis catalysis

- Direct synthesis of DME from syngas: catalytic bed optimization CZA: $\gamma$ -Al<sub>2</sub>O<sub>3</sub>

CZA_comm	$\gamma$ -Al <sub>2</sub> O <sub>3</sub>	m:a (CZA_comm: $\gamma$ -Al <sub>2</sub> O <sub>3</sub> )
90 %	10 %	90:10
50 %	50 %	50:50
10 %	90 %	10:90

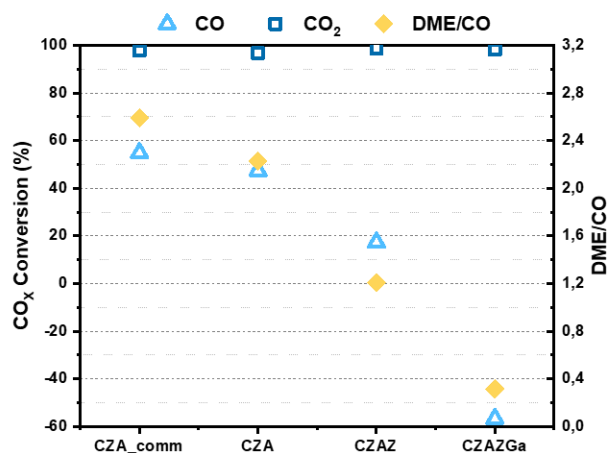
- The highest DME productivity was obtained with the m:a= 50:50 at 270 °C, 50 bar and 5000 h<sup>-1</sup>
- Stability test during 270 h: the CO conversion decreased during the TOS, but the CO<sub>2</sub> conversion remains at 10%
- The highest DME selectivity obtained with the m:a = 10:90



# Sorption-enhanced DME synthesis catalysis

- Sorption enhanced DME synthesis from syngas:

Catalytic bed CZA: $\gamma$ -Al<sub>2</sub>O<sub>3</sub>:3A



Removing H<sub>2</sub>O results in high CO<sub>2</sub> conversion and DME production

Very high DME production

Low CO<sub>2</sub> in products  
↓  
Easier separation  
DME/CO<sub>2</sub> downstream

Reverse Water Gas Shift Catalyst



Highest CO production  
Highest non converted CH<sub>3</sub>OH  
Lowest DME production

275 °C; 25 bar; 1080 h<sup>-1</sup>; CO<sub>2</sub>/CO=2; CO/CO<sub>2</sub>/H<sub>2</sub>= 9/18/73 (v/v)

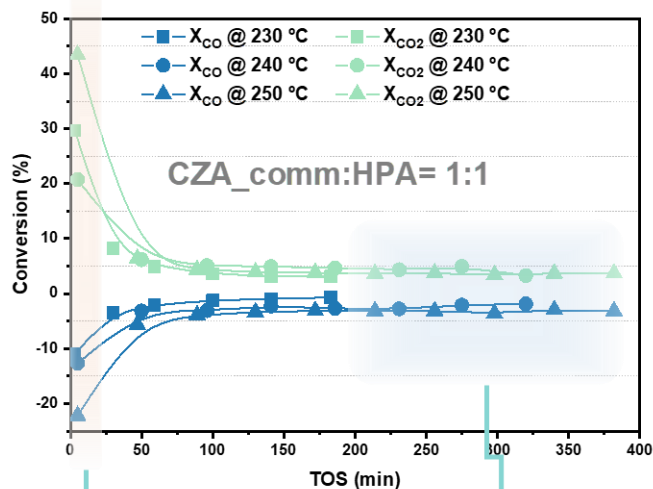


# Sorption-enhanced DME synthesis catalysis

- Sorption enhanced DME synthesis from syngas:

catalytic bed CZA: $\gamma$ -HWSi/TiO<sub>2</sub>:3A

230-240-250 °C; 25 bar; 5000 h<sup>-1</sup>; CO<sub>2</sub>/CO=1.9; CO/CO<sub>2</sub>/H<sub>2</sub>= 9/18/73 (v/v)

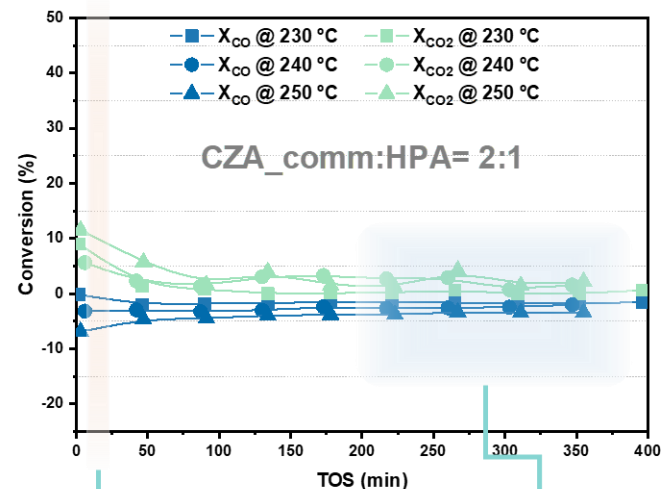


250 °C

**% DME: 40**  
**% CH<sub>3</sub>OH: 49**

250 °C

**% DME: 26**  
**% CH<sub>3</sub>OH: 71**



250 °C

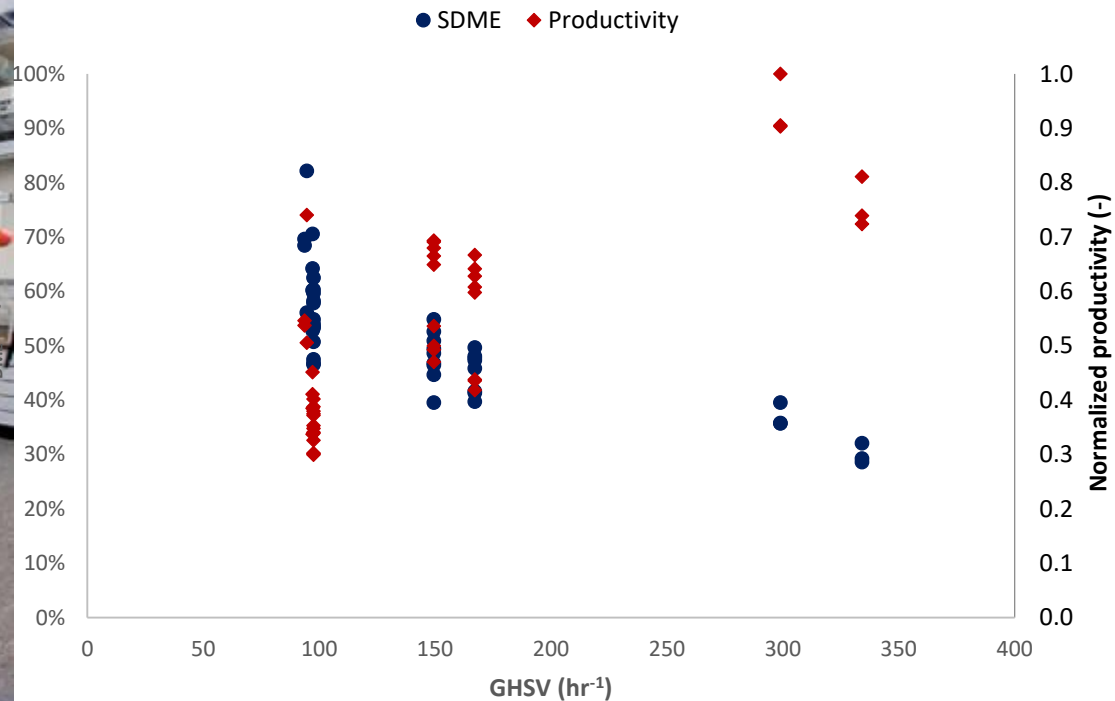
**% DME: 7**  
**% CH<sub>3</sub>OH: 30**

250 °C

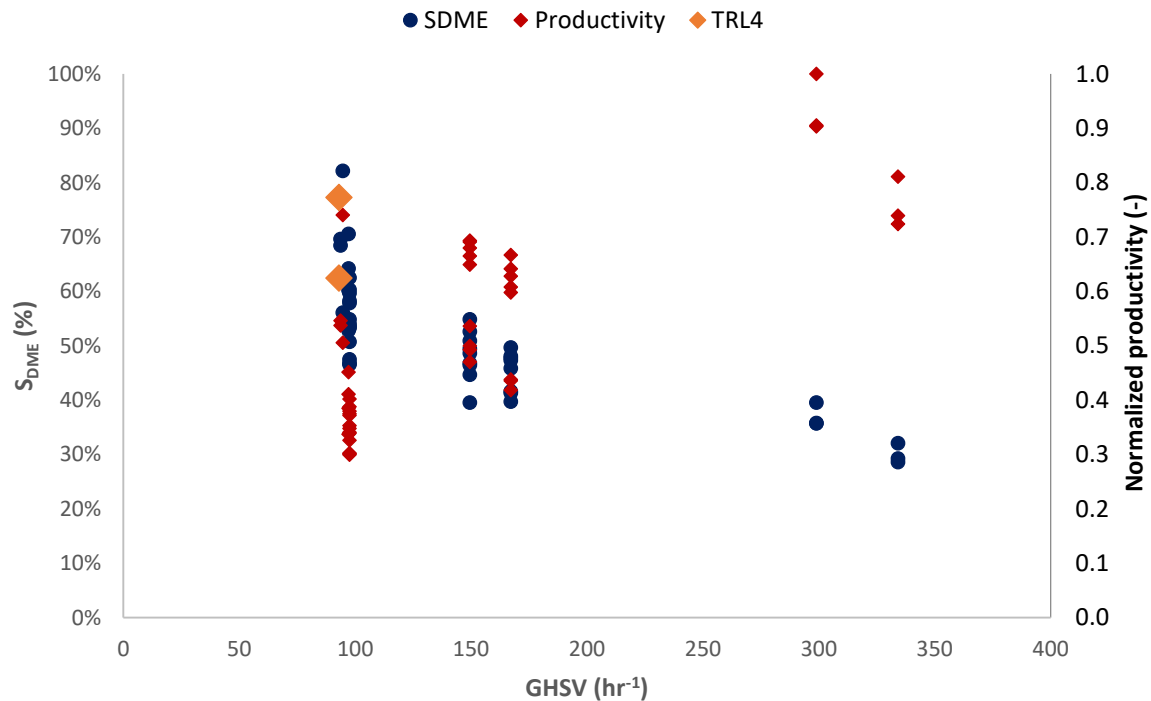
**% DME: 7**  
**% CH<sub>3</sub>OH: 86**



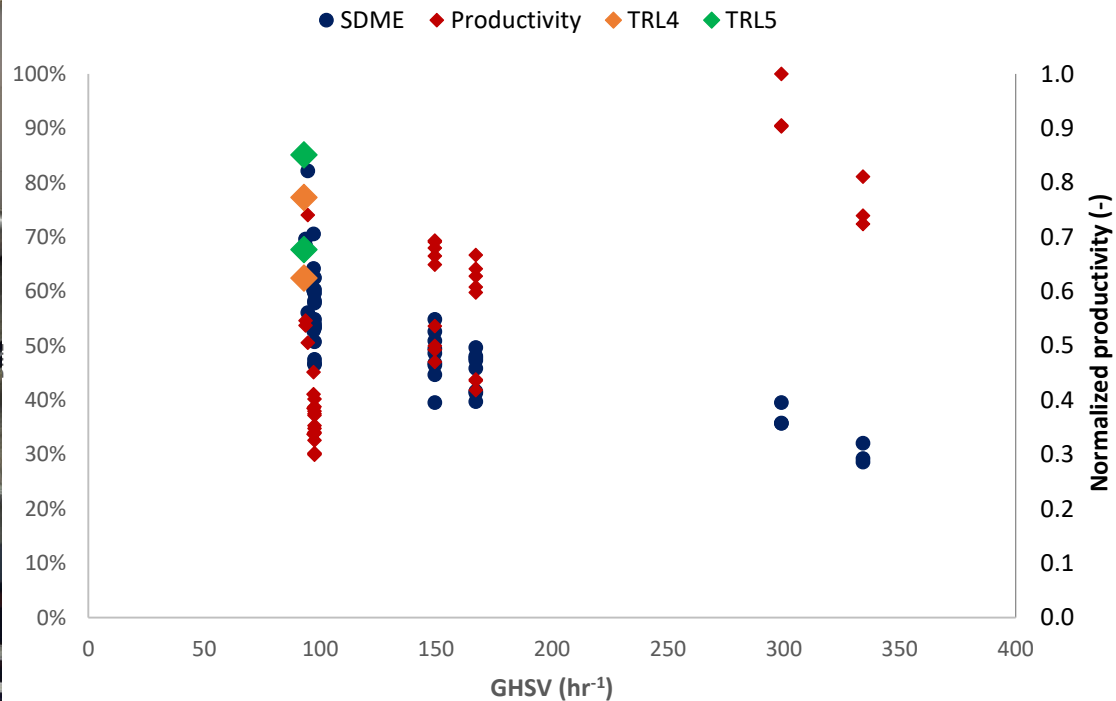
# SEDMES: Experimental validation



# SEDMES: Experimental validation

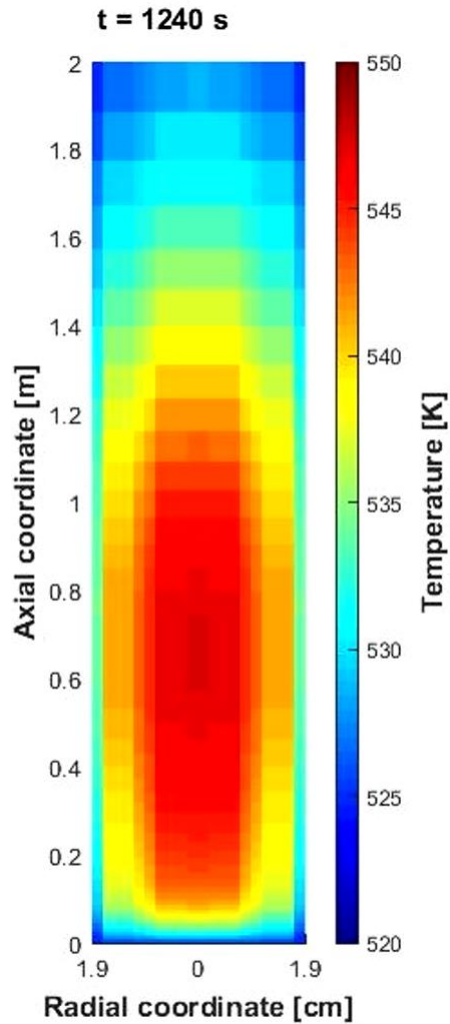


# SEDMES: Experimental validation

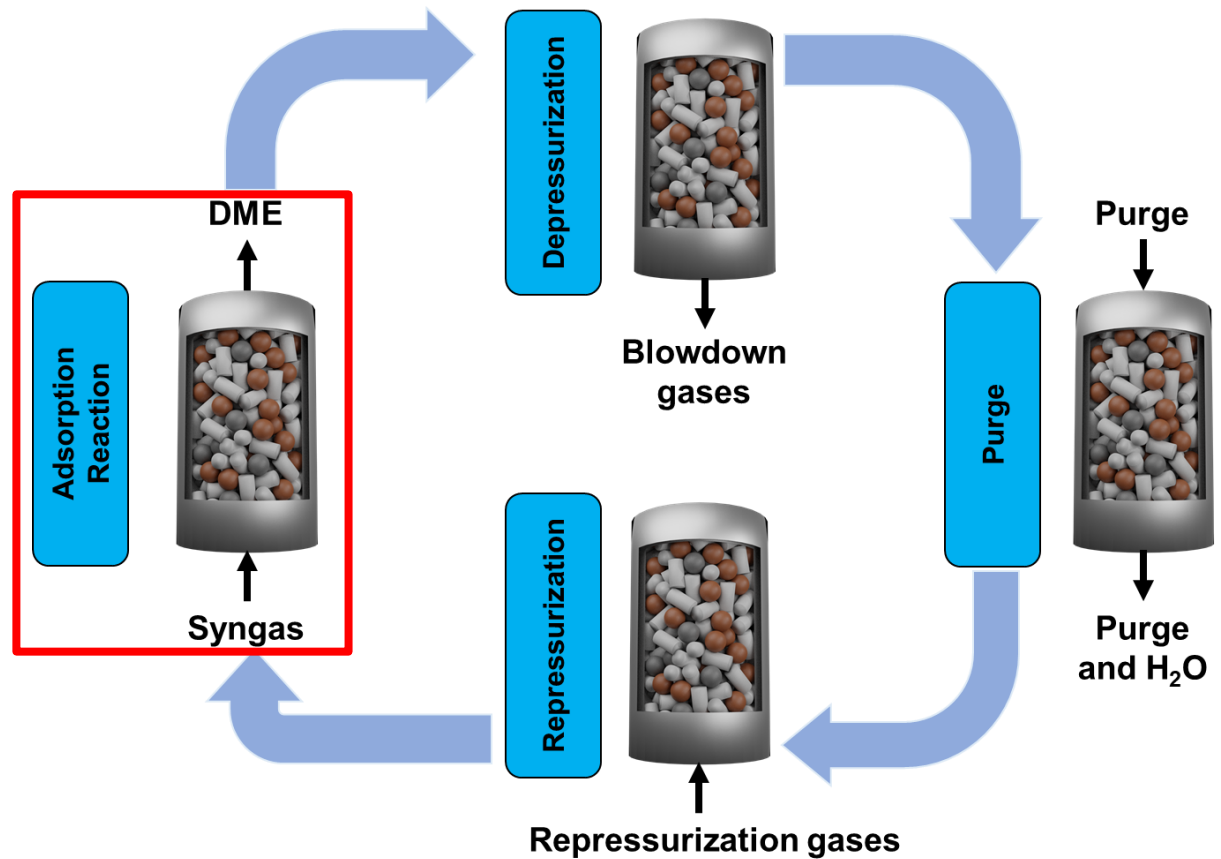




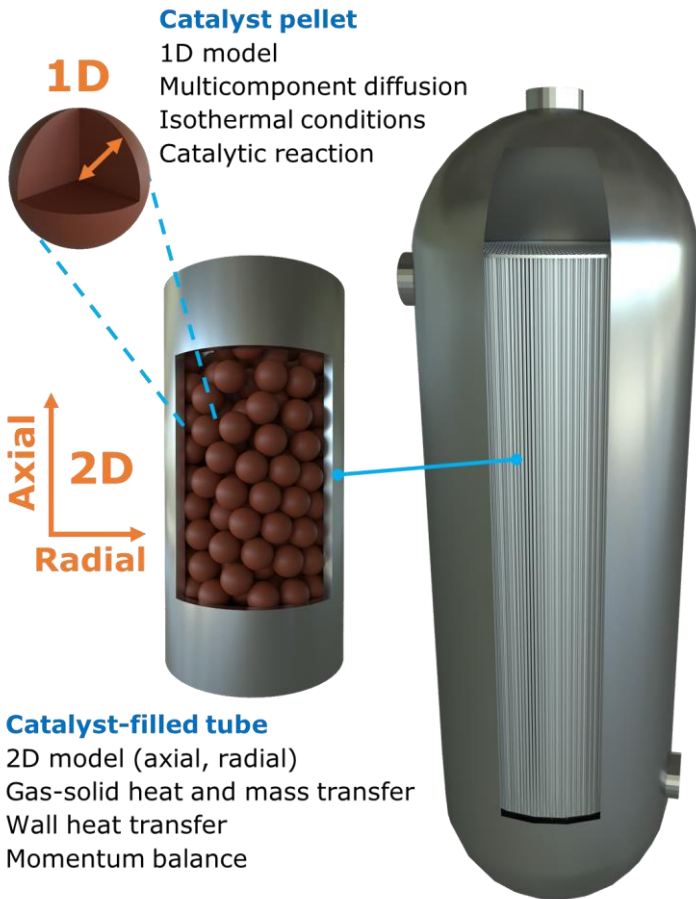
# SEDMES: 2D reactor modelling



## Pressure Swing Adsorption (PSA) cycle

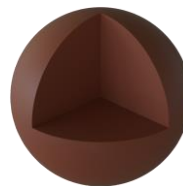


# Reactor model

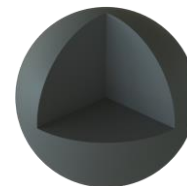


## SEDMES reactor:

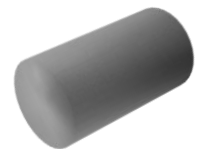
- Multitubular fixed bed reactor externally cooled
- Dynamic conditions
- 2D single tube heterogeneous model
- 1D catalyst pellet model
- Linear Driving Force for adsorbent pellet



Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>



γ-Al<sub>2</sub>O<sub>3</sub>

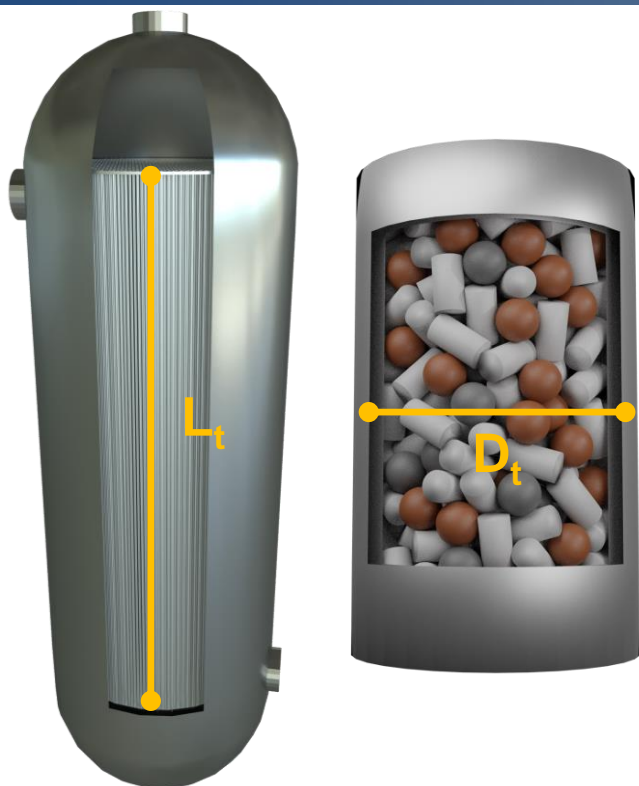


LTA zeolite



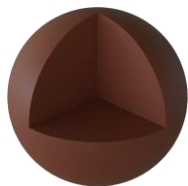


# SEDMES reactor analysis and design

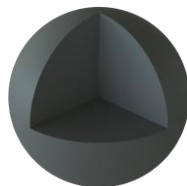


$$\alpha = \frac{CO}{CO + CO_2}$$

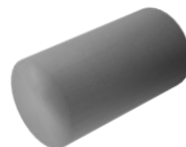
$$M = \frac{H_2 - CO_2}{CO + CO_2}$$



Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>



γ-Al<sub>2</sub>O<sub>3</sub>



LTA zeolite

## Input parameters

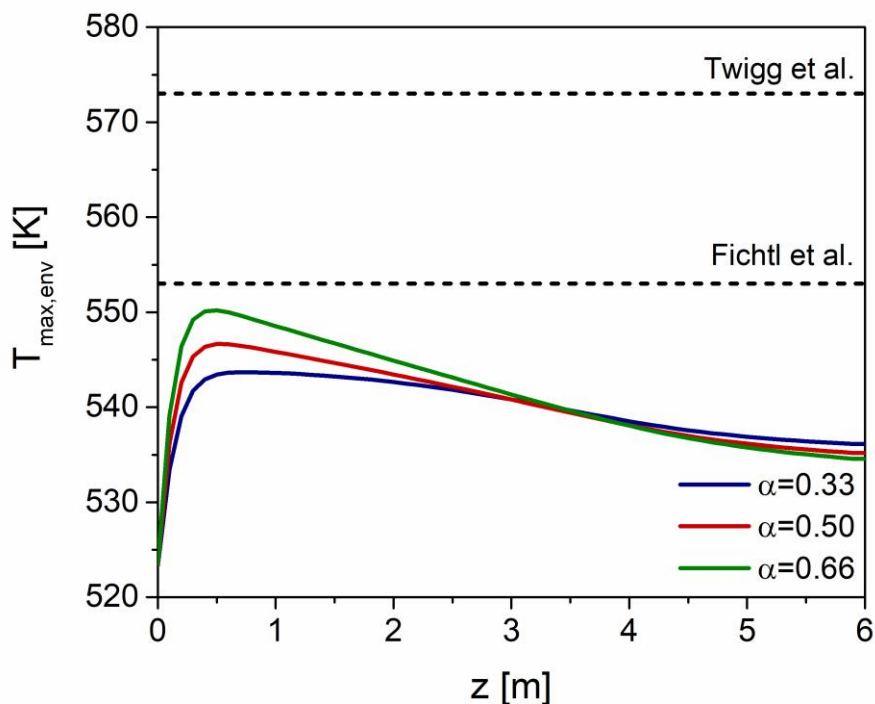
T <sub>inlet</sub>	523 K
T <sub>cool</sub>	523 K
P <sub>inlet</sub>	25 bar
GHSV	140 h <sup>-1</sup>
Ads:Cat.	4 : 1 w/w
CZA:γ-Al <sub>2</sub> O <sub>3</sub>	1 : 1 w/w
L <sub>t</sub>	6 m
M	2

## Analyzed parameters

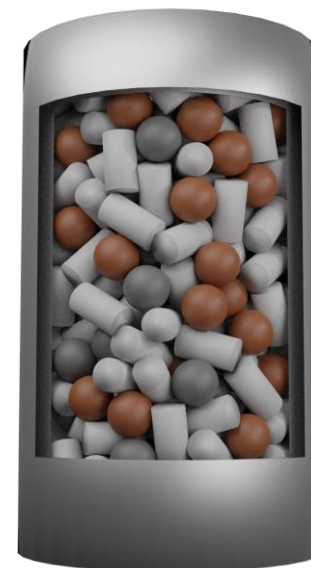
α	0.33-0.66
D <sub>t</sub>	25.6-46.6 mm



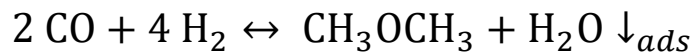
# SEDMES reactor: effect of $\alpha = \text{CO}/\text{CO}_x$ on thermal stresses



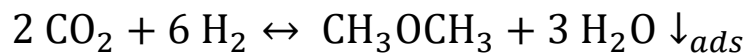
M. V. Twigg et al., Appl. Catal. A Gen. 212 (2001) 161–174.  
 M.B. Fichtl et al, Appl. Catal. A Gen. 502 (2015) 262–270.



**Ads./Cat. = 4/1 w/w**



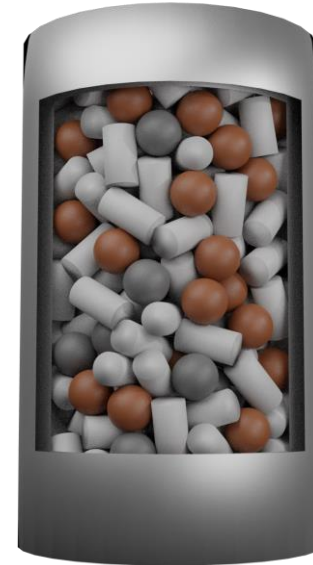
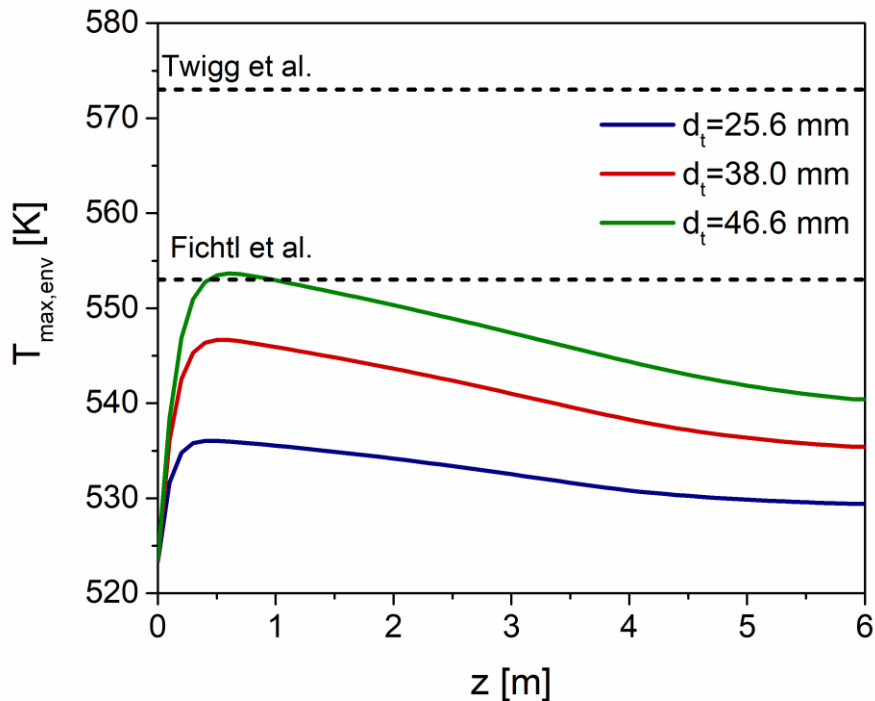
$$\Delta H_r^0 = -250.0 \text{ kJ/mol}_{DME}$$



$$\Delta H_r^0 = -259.7 \text{ kJ/mol}_{DME}$$

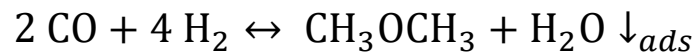


# SEDMES reactor: effect of the tube diameter on thermal stresses

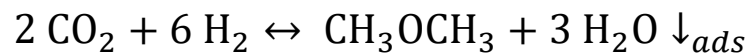


**Ads./Cat. = 4/1 w/w**

S. Guffanti et al., NGCS12, (2019), San Antonio (Texas – USA). → **25.6 mm**



$$\Delta H_r^0 = -250.0 \text{ kJ/mol}_{DME}$$



$$\Delta H_r^0 = -259.7 \text{ kJ/mol}_{DME}$$



## Sub conclusions

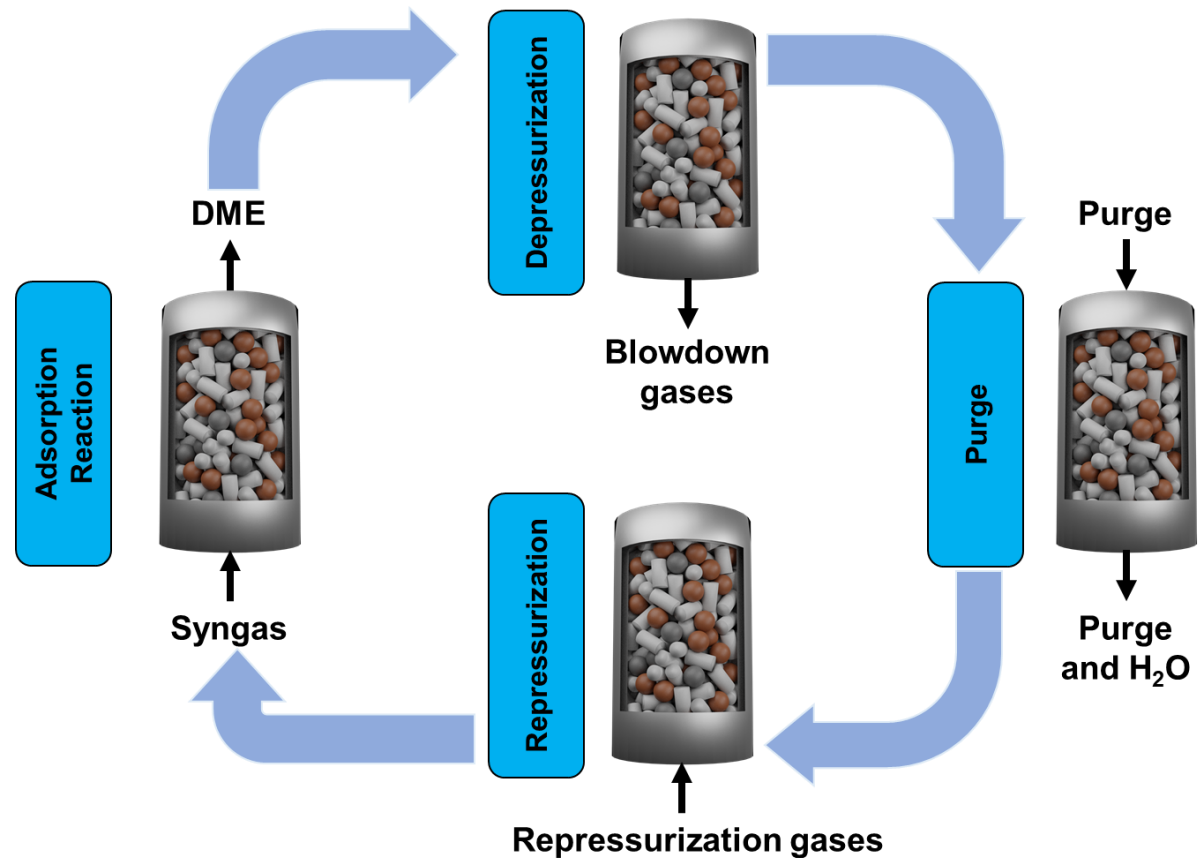
- **A SEDMES 2D reactor model has been developed and validated against bench scale experimental data (TRL4).**
- **Model results confirm high DME yields for SEDMES, independently of syngas CO/CO<sub>x</sub> ratio, which is particularly advantageous at high CO<sub>2</sub> content.**
- **The thermal dilution of catalyst in adsorbent material (1/4 w/w) allows to operate with larger tube diameters with respect to the conventional synthesis.**



# SEDMES: Cycle design

- SEDMES
- Cyclic reactor model
- Validated at TRL4

## Pressure Swing Adsorption (PSA) cycle



# SEDMES: Cycle design

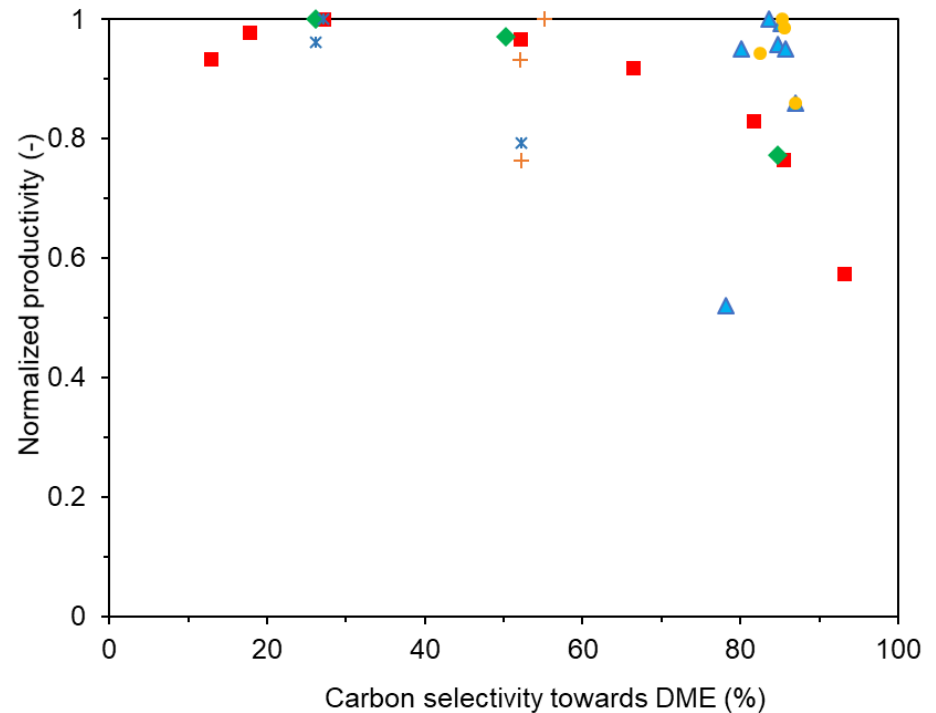
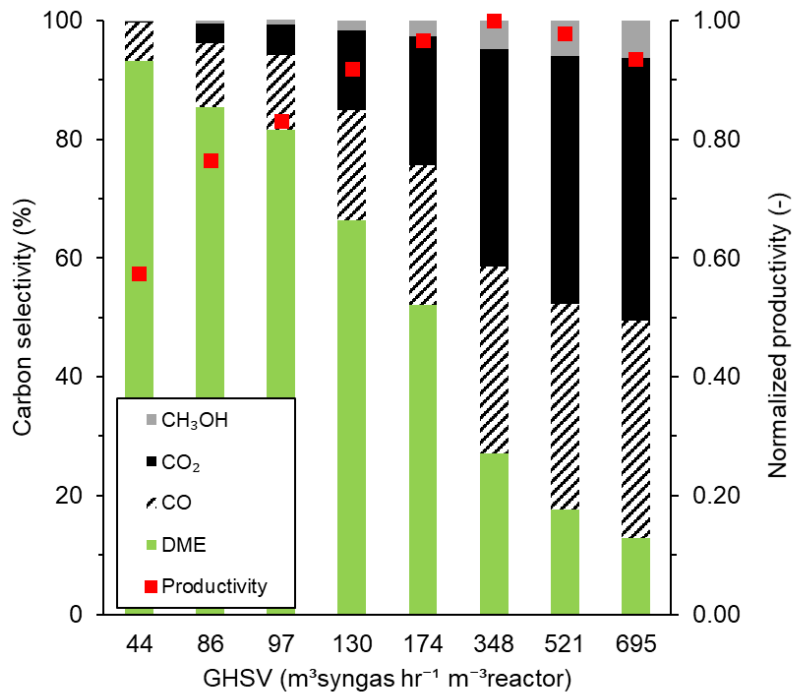
Column 1	ADS	PEQDN	BD	PURGE	PEQUP	REP
Column 2	REP	ADS	PEQDN	BD	PURGE	PEQUP
Column 3	PEQUP	REP	ADS	PEQDN	BD	PURGE
Column 4	PURGE	PEQUP	REP	ADS	PEQDN	BD
Column 5	BD	PURGE	PEQUP	REP	ADS	PEQDN
Column 6	PEQDN	BD	PURGE	PEQUP	REP	ADS

## Optimization parameters:

- Gas hourly space velocity during adsorption, purge and repressurization step
- Cycle time
- Pressure equalization step(s)
- Gas recycling
- Operating conditions per step
- Adjusting boundary conditions



# SEDMES: Cycle design



Typical for sorption-enhanced processes trade-off between carbon selectivity towards DME and productivity



TNO



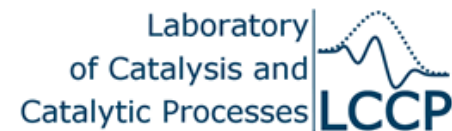
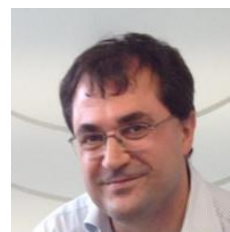
# SEDMES: Conclusions

- Separation-enhanced synthesis technology offers intensified processes for economic valorisation of CO<sub>2</sub>-rich syngas
- Sorption-enhanced DME synthesis, SEDMES, has been developed using commercially available materials
- Novel catalysts show promising results: Especially HPA shows high activity for selective DME synthesis
- Validated modelling frameworks have allowed to design the SEDMES reactor and optimise the SEDMES process for Fledged case
- SEDMES technology validated in relevant multicolumn, environment (TRL5)





# Contact information



**POLITECNICO**  
MILANO 1863





*This project has received funding from the European Union's  
Horizon 2020 research and innovation programme  
under grant agreement No 727600*

